



BUILDING ENERGY 15

MARCH 3-5, 2015 AT THE SEAPORT WORLD TRADE CENTER

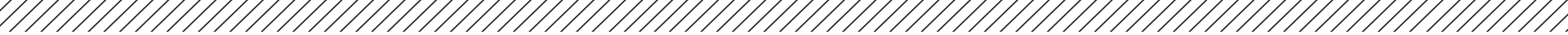
AIA Provider: Northeast Sustainable Energy Association

Provider Number: G338

Sensible Solutions to Latent Problems

Aubrey Gewehr, David White

March 5 2015



Credit(s) earned on completion of this course will be reported to **AIA CES** for AIA members. Certificates of Completion for both AIA members and non-AIA members are available upon request.

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Questions related to specific materials, methods, and services will be addressed at the conclusion of this presentation.

This course is registered with **AIA CES**



Course Description

Low-load homes struggle with summertime humidity more than conventional homes, and the Northeast isn't getting any less tropical. Let's get ready. We will consider how latent and sensible loads differ for low-load homes, how to calculate required equipment performance, and what our equipment options are. After reviewing the basics of the psychrometric chart, we'll use it as our playbook, loading it with zippy-looking graphics galore. We will also present monitoring from recently built low-load homes.

Learning Objectives

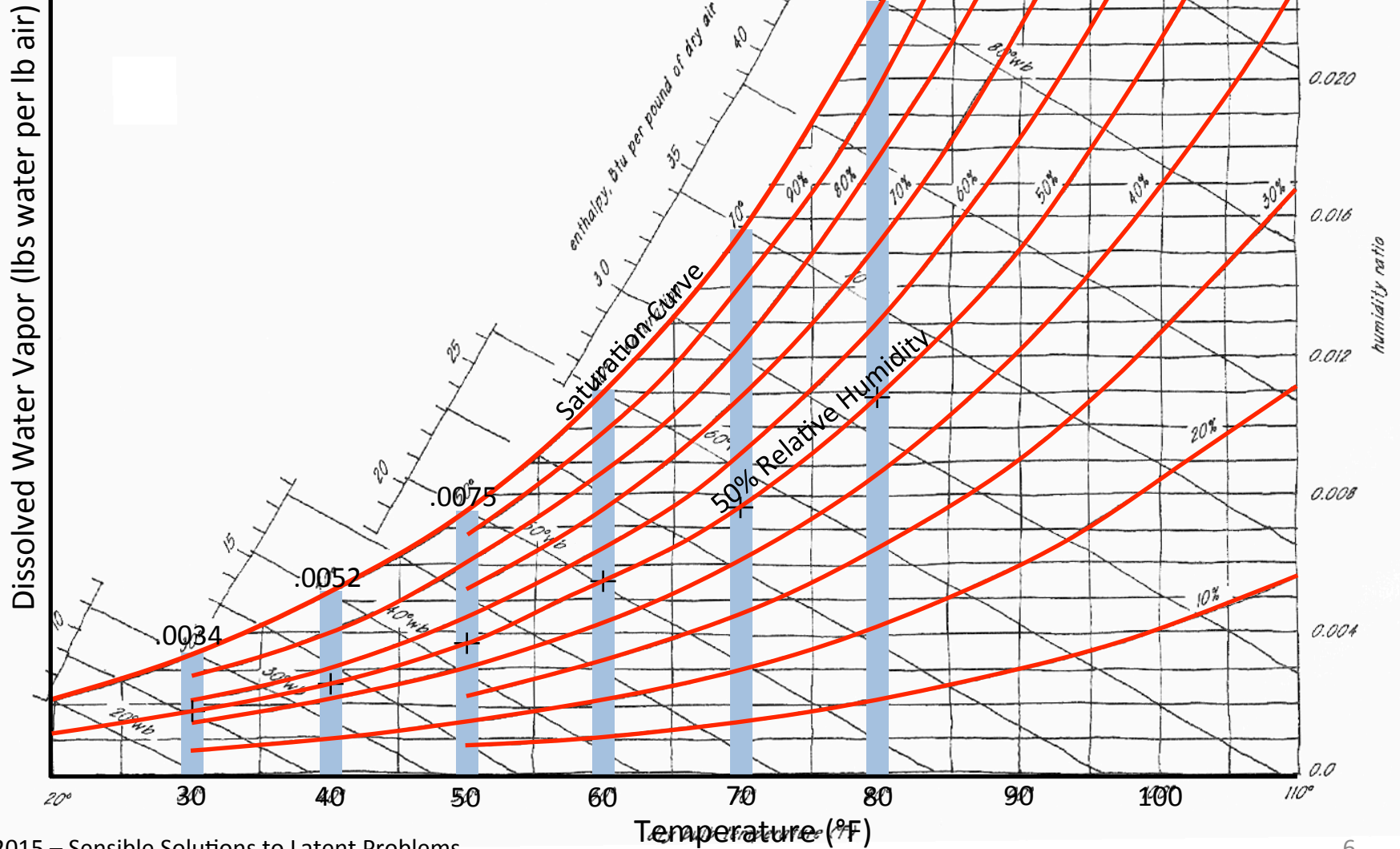
At the end of the this course, participants will be able to:

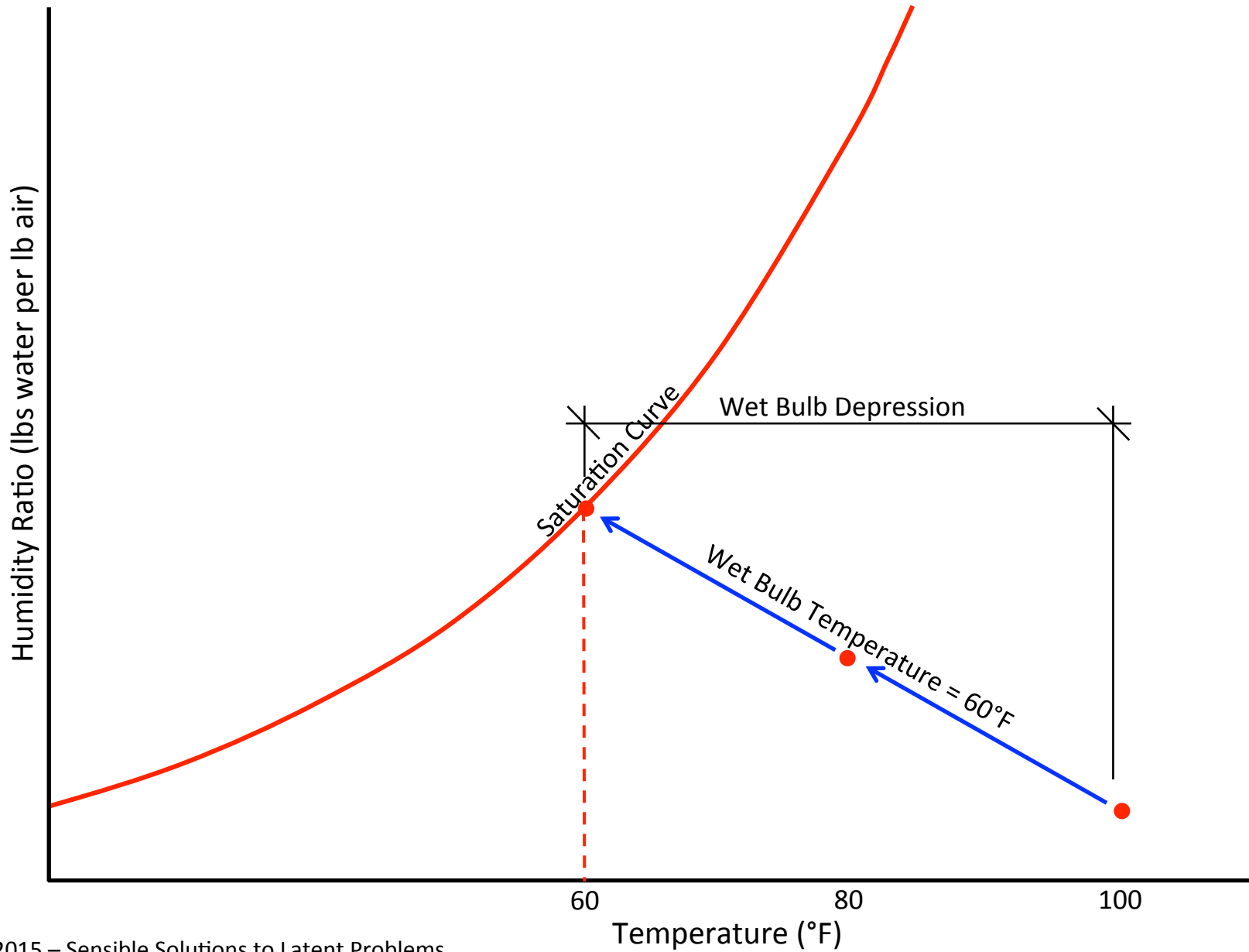
- 1) Understand the difference between sensible and latent loads.
- 2) Be better equipped to evaluate mechanical system proposals for high-efficiency residential buildings.
- 3) Distinguish between relative humidity and total moisture content of air.
- 4) Use the psychrometric chart.

This concludes The American Institute of Architects
Continuing Education Systems Course

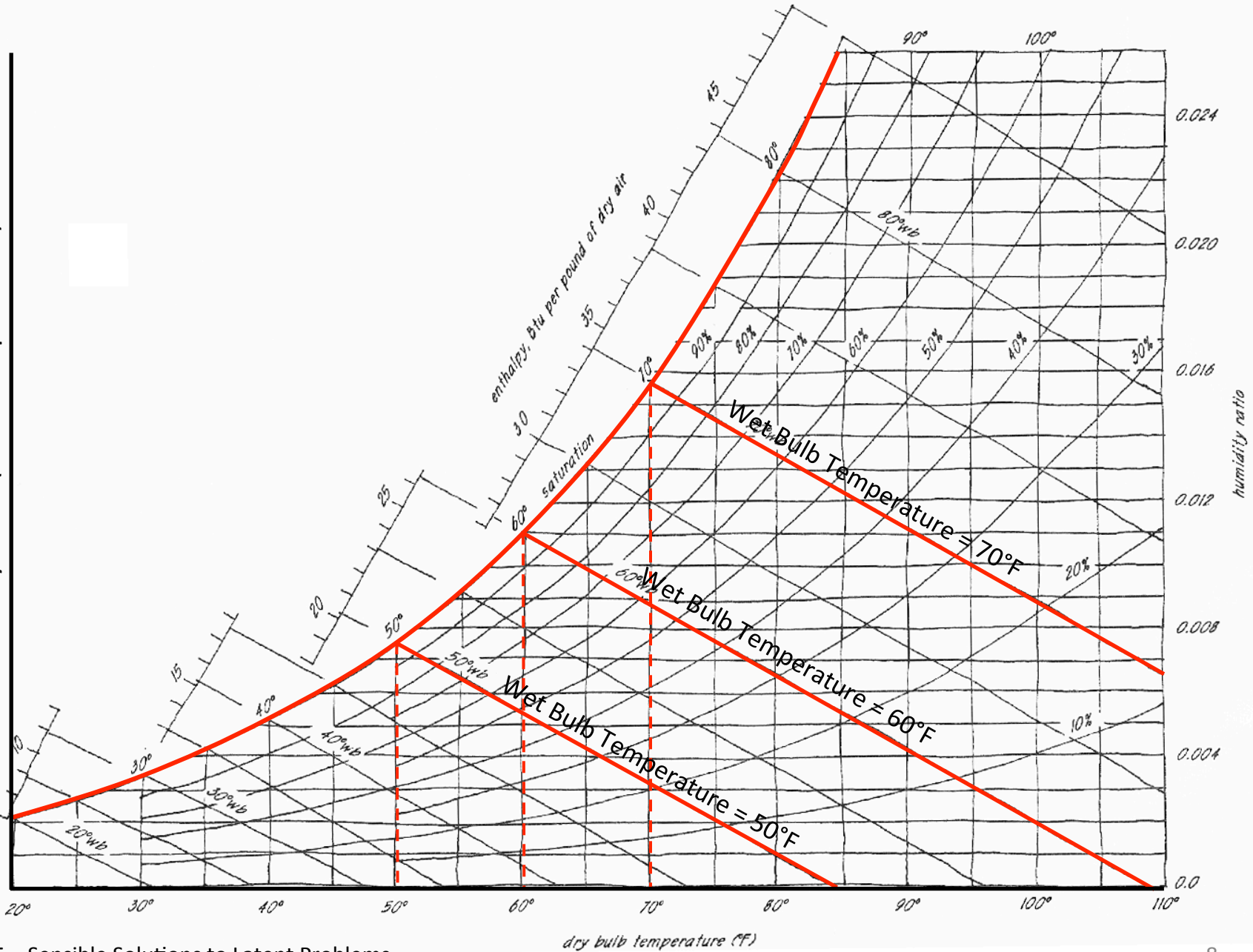


Psychrometric Chart

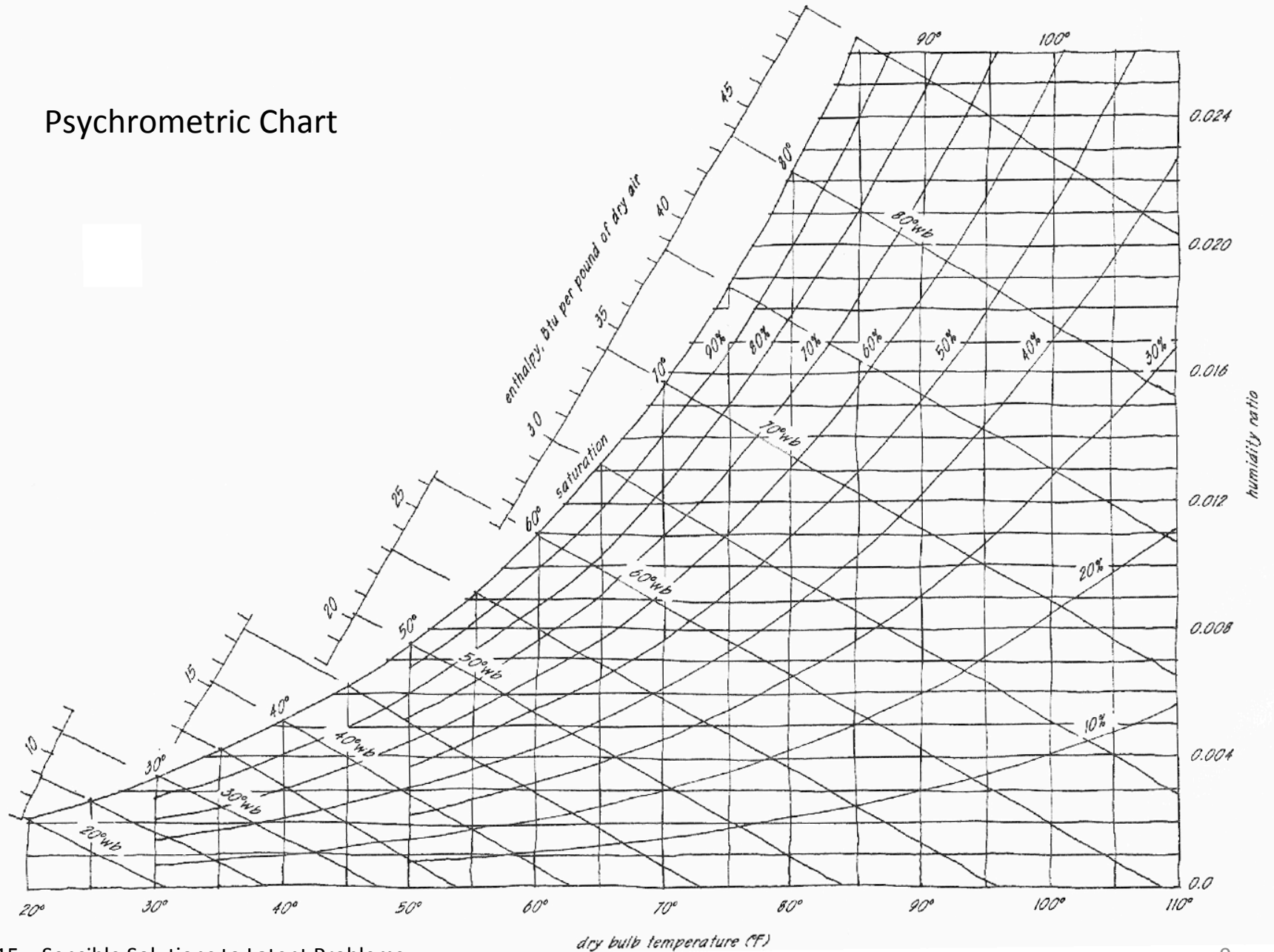


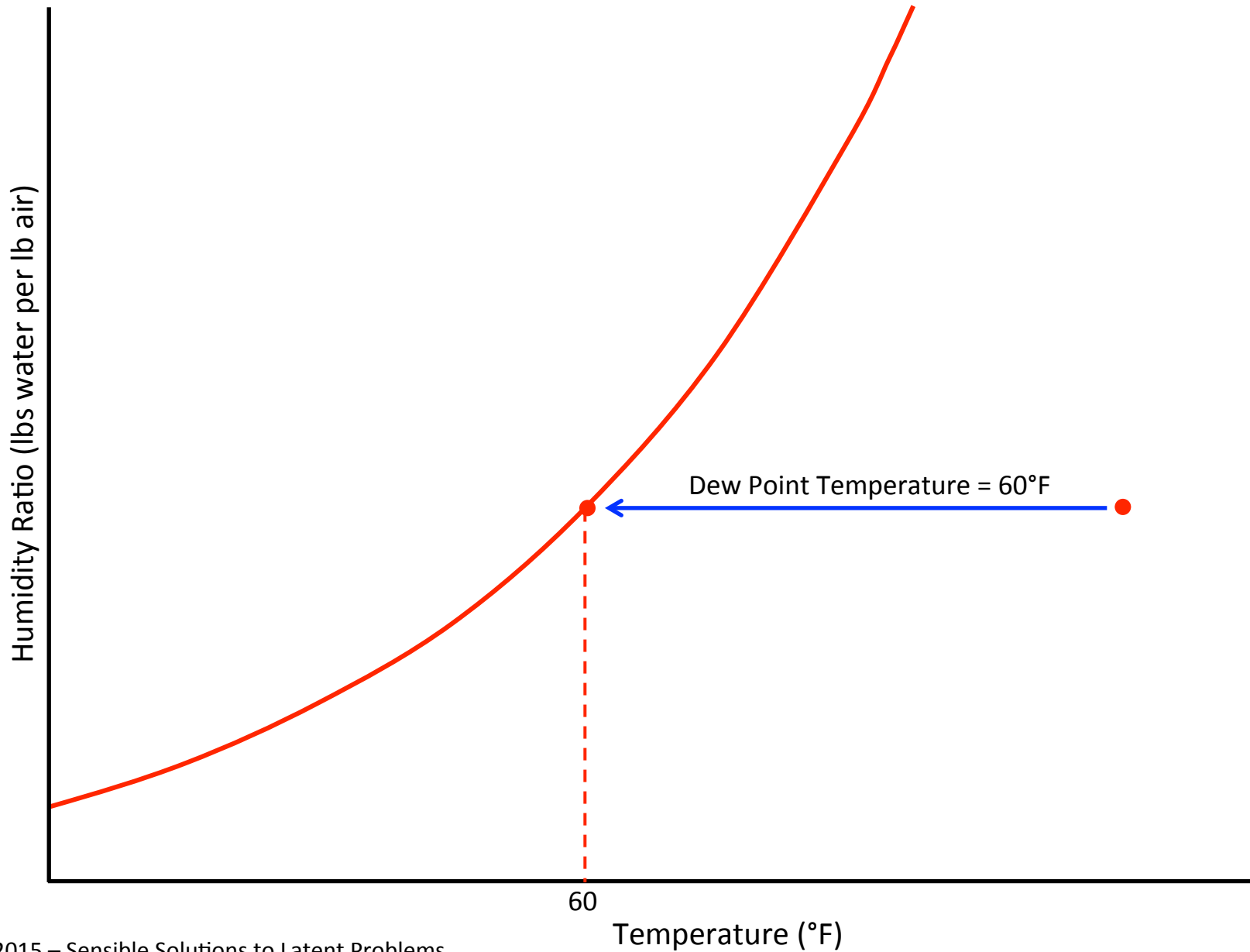


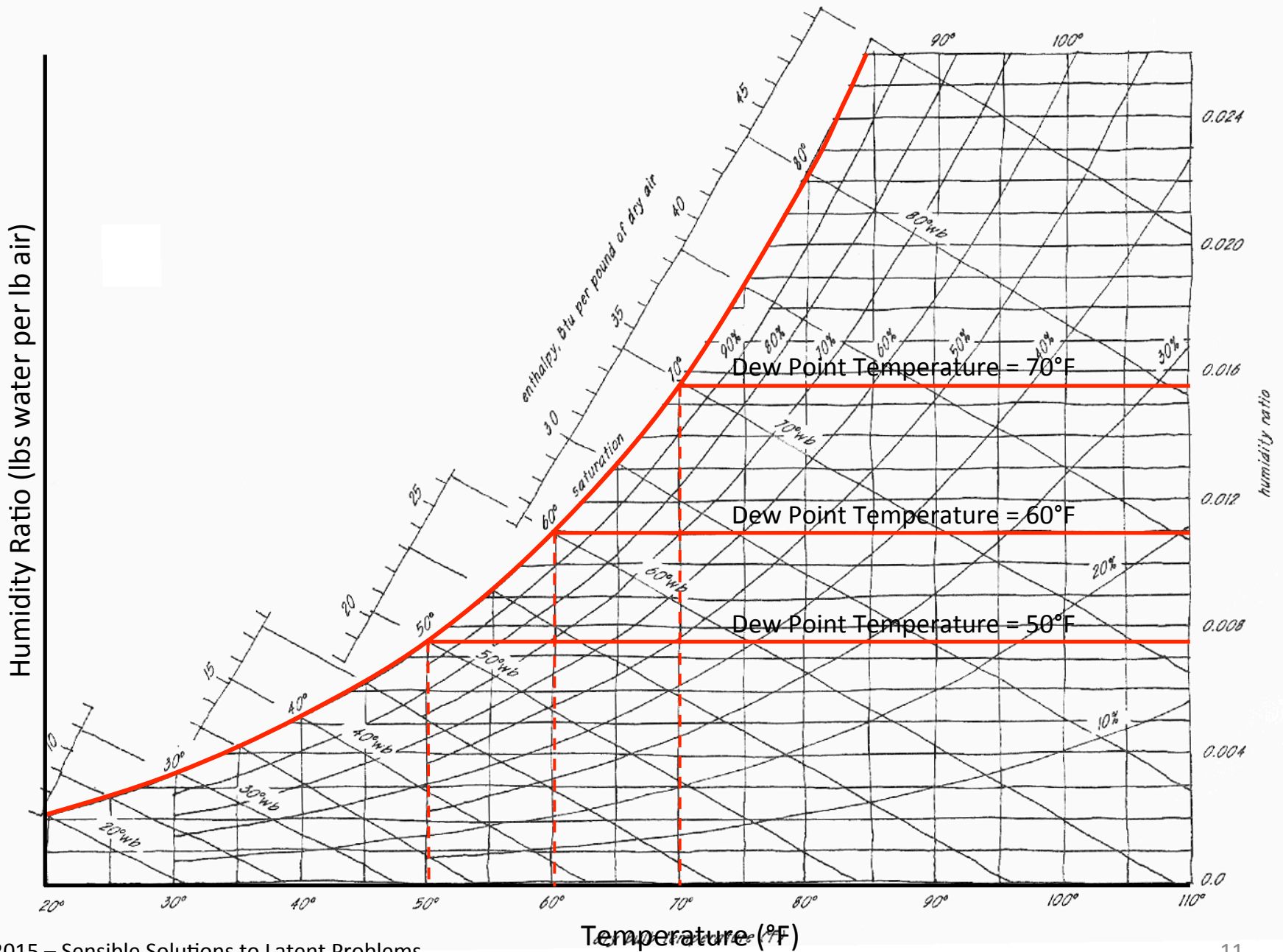
Humidity Ratio (lbs water per lb air)

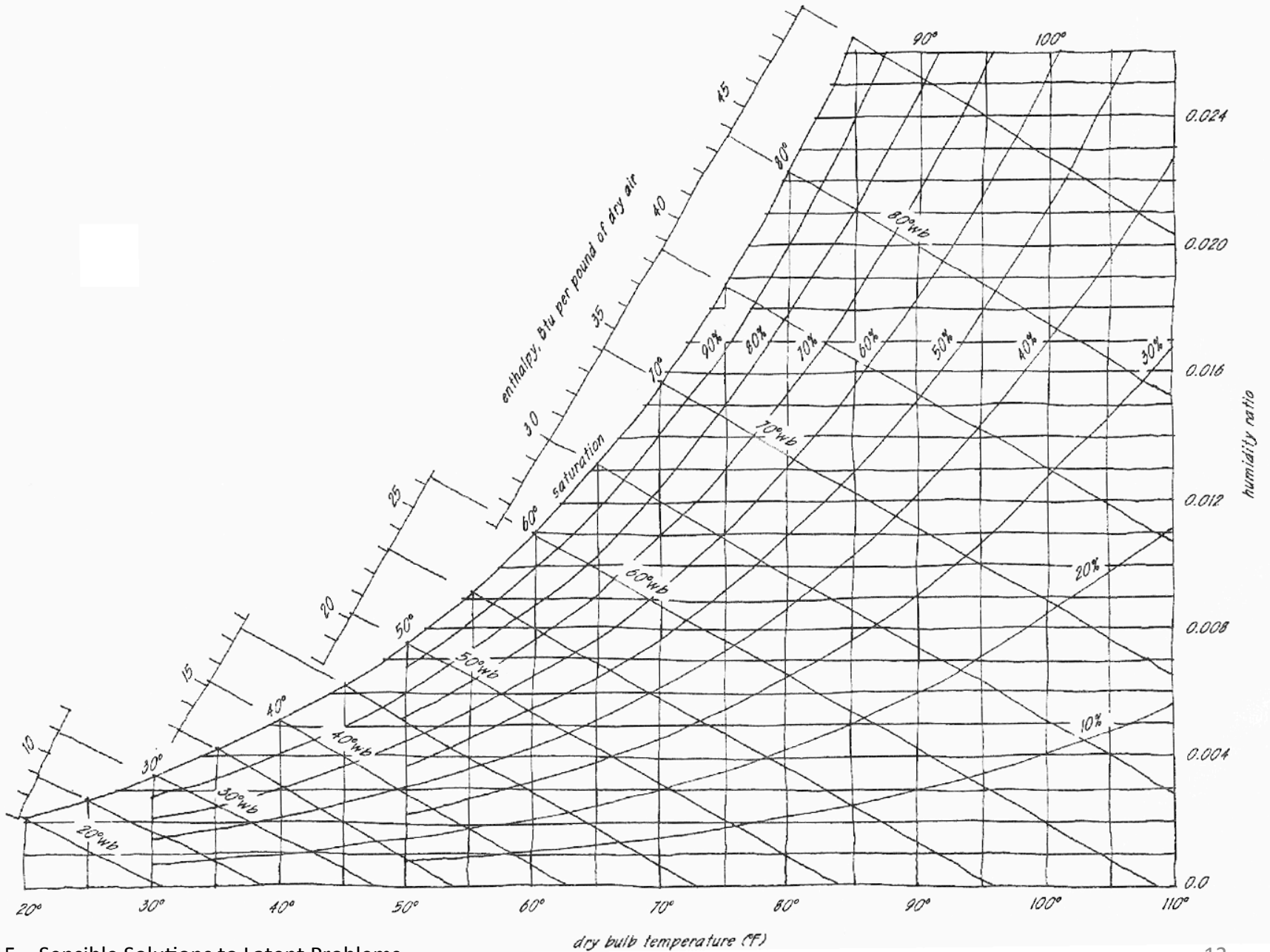


Psychrometric Chart



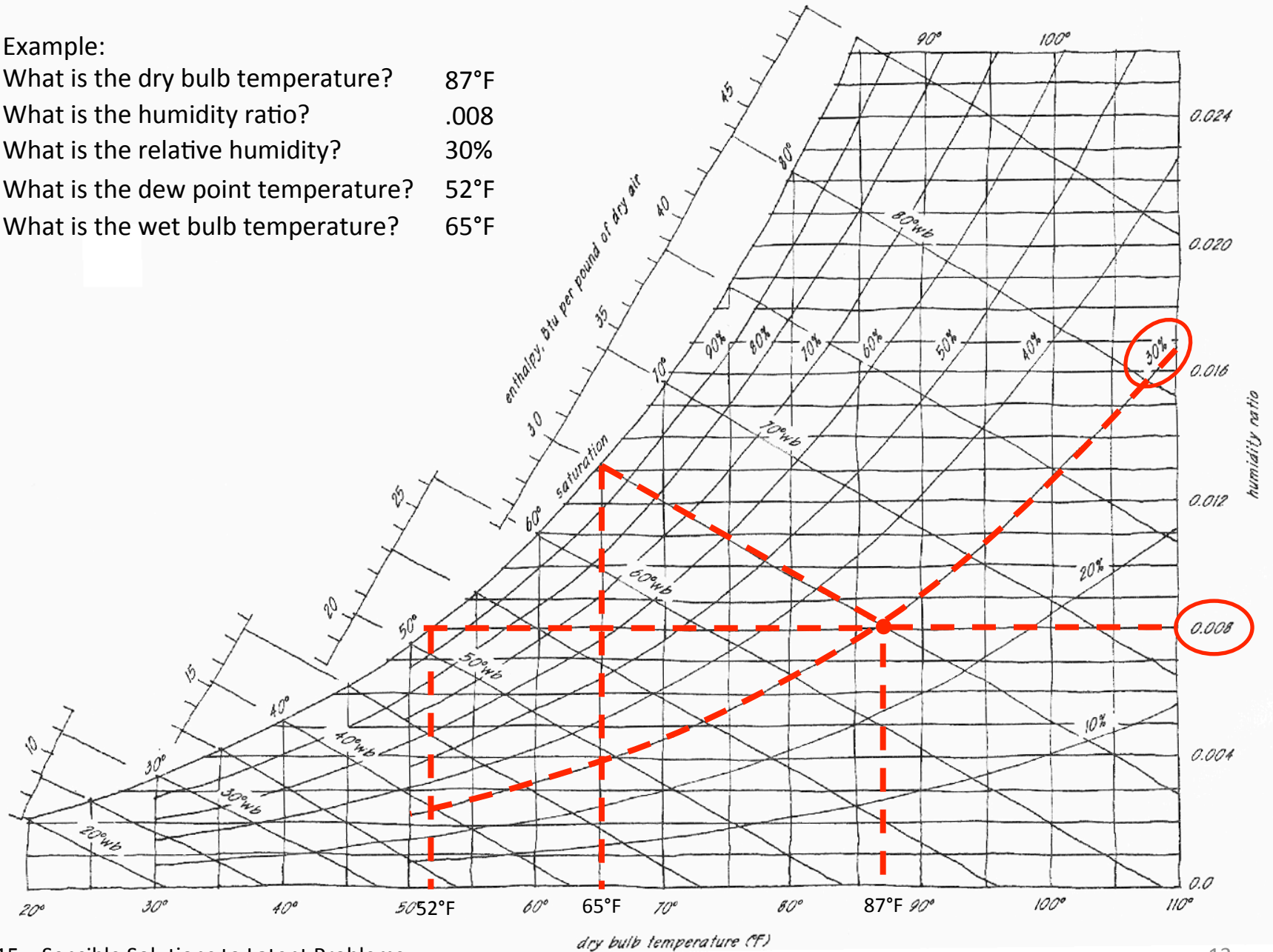




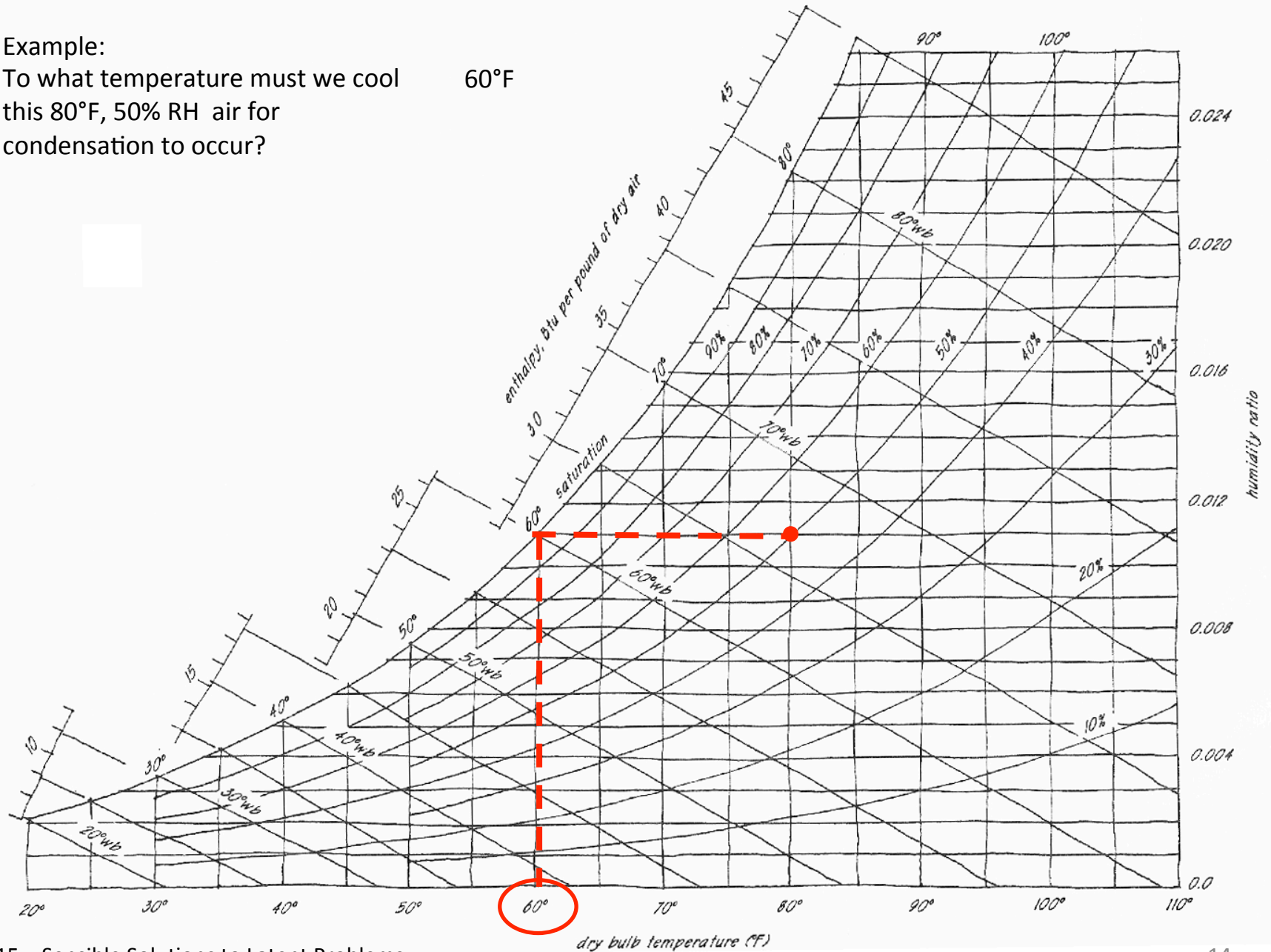


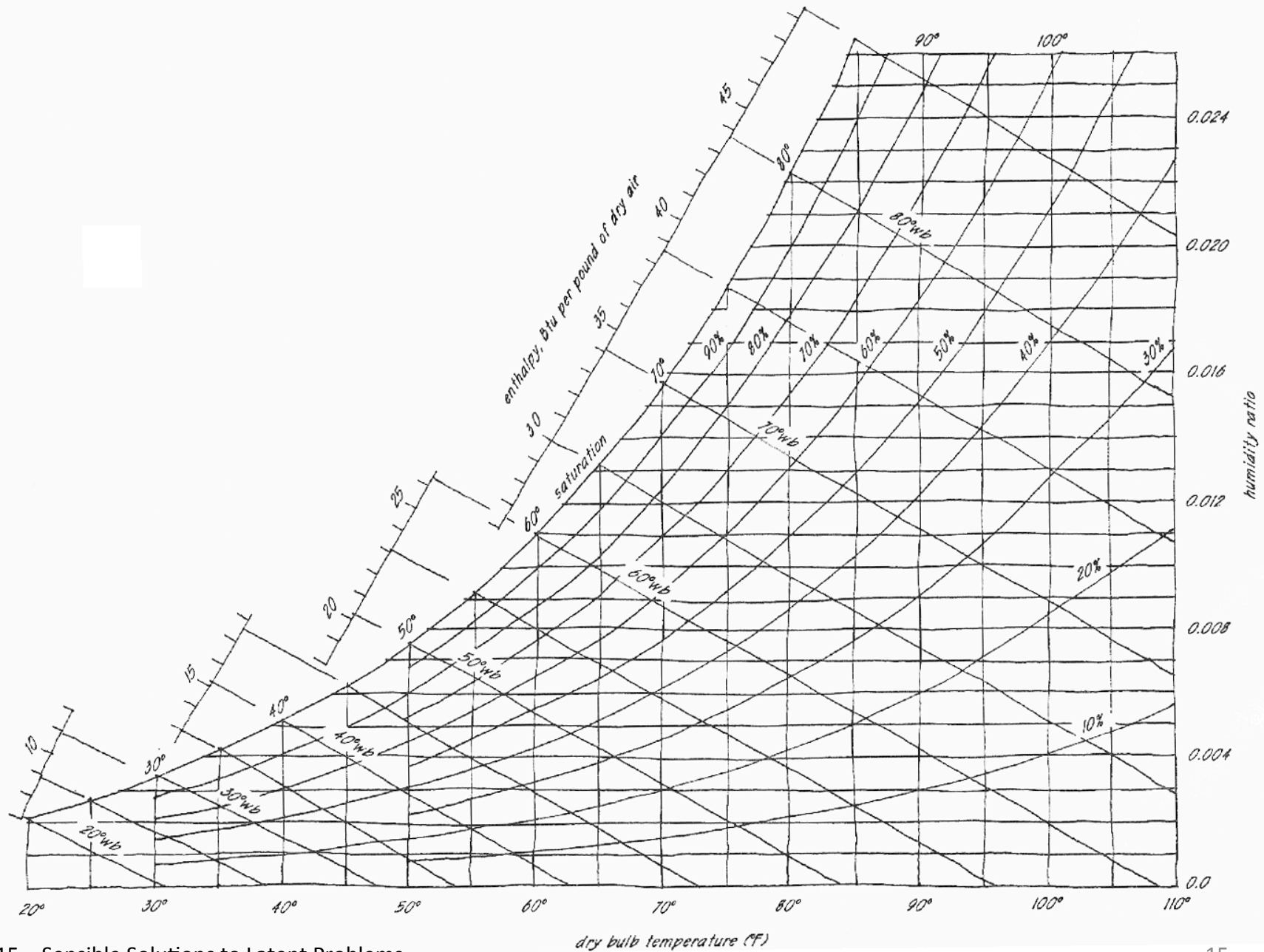
Example:

What is the dry bulb temperature? 87°F
What is the humidity ratio? .008
What is the relative humidity? 30%
What is the dew point temperature? 52°F
What is the wet bulb temperature? 65°F

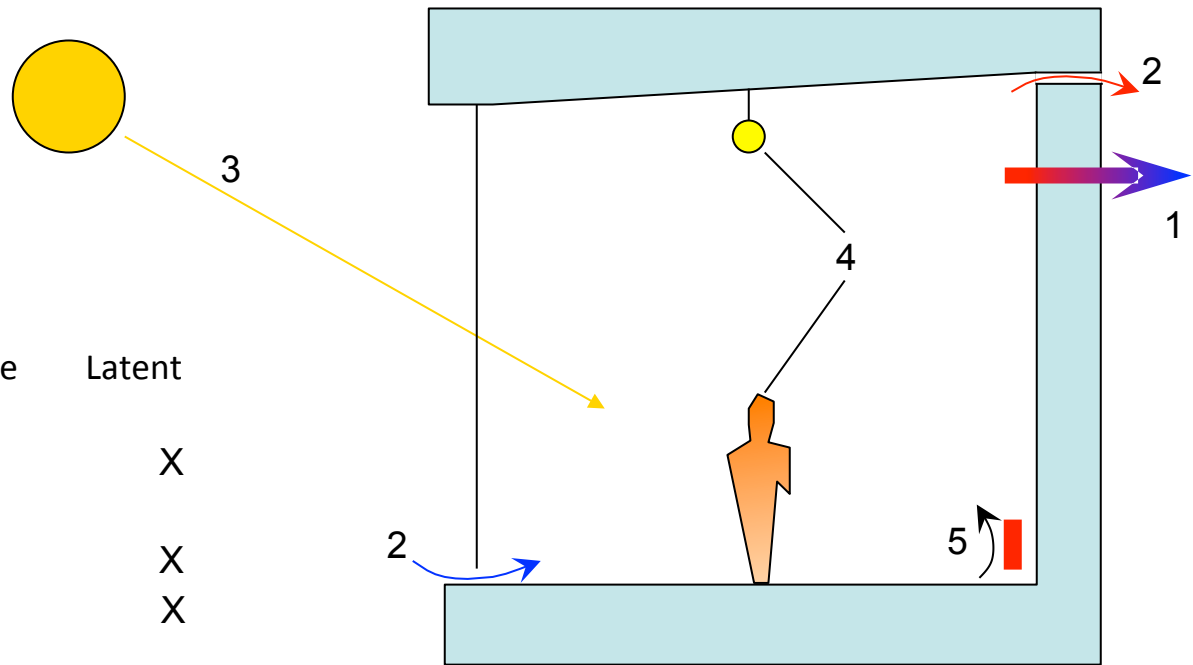


Example:
To what temperature must we cool
this 80°F, 50% RH air for
condensation to occur?





		Sensible	Latent
1	Transmission	X	
2	Infiltration/Ventilation	X	X
3	Solar Gain	X	
4	Internal Gain	X	X
5	Artificial Heating/Cooling	X	X



LOT 1
 "WOODLAND ACRES SUBDIVISION"
 FILED IN THE ORANGE COUNTY CLERK'S OFFICE
 AS MAP #165-98
 LANDS NOW OR FORMERLY SURVEYED
 LIBER 2493 PAGE 193
 T.M. SECTION 18 - BLOCK 4 - LOT 77.1

LOT 13
 LANDS NOW OR FORMERLY ALZAMORA
 LIBER 8054 PAGE 163
 T.M. SECTION 18 - BLOCK 4 - LOT 31






LOT 1 SUPERVISOR'S OFFICE
 FILED IN THE ORANGE COUNTY CLERK'S OFFICE
 AS MAP #165-98
 LANDS NOW OR FORMERLY SURVEYED
 LIBER 2493 PAGE 193
 T.M. SECTION 18 - BLOCK 4 - LOT 77.1

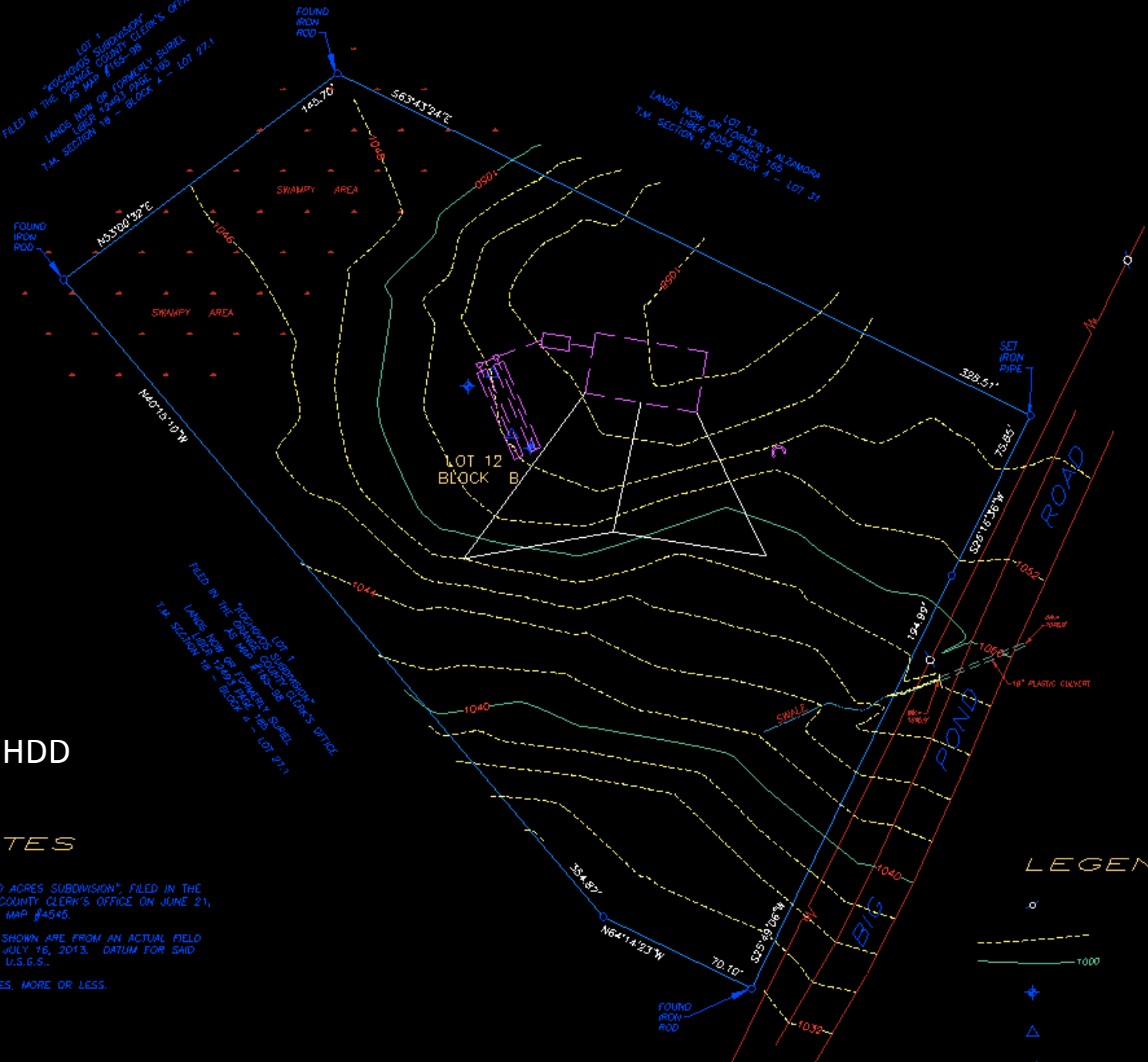
6,000 HDD

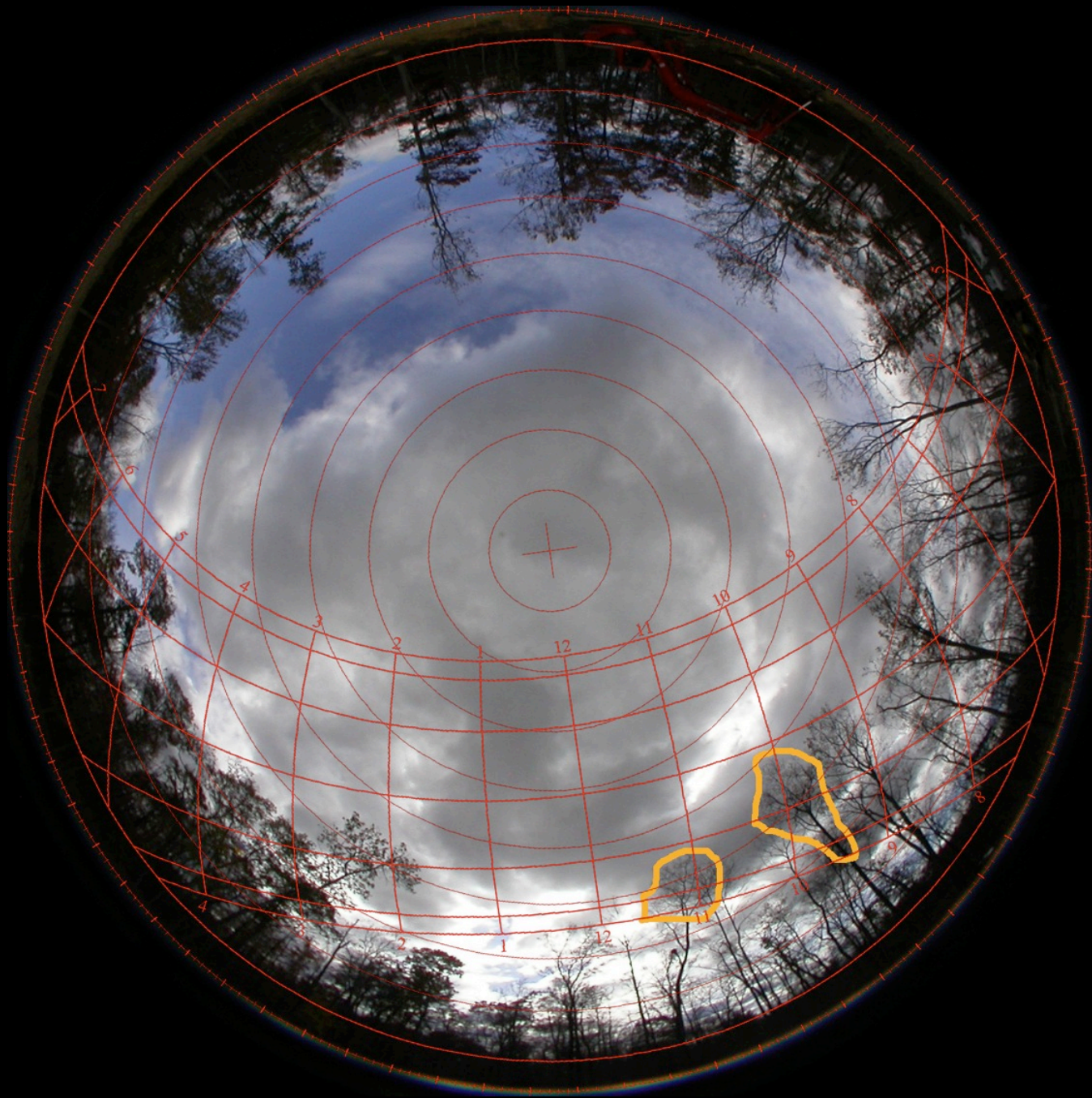
NOTES

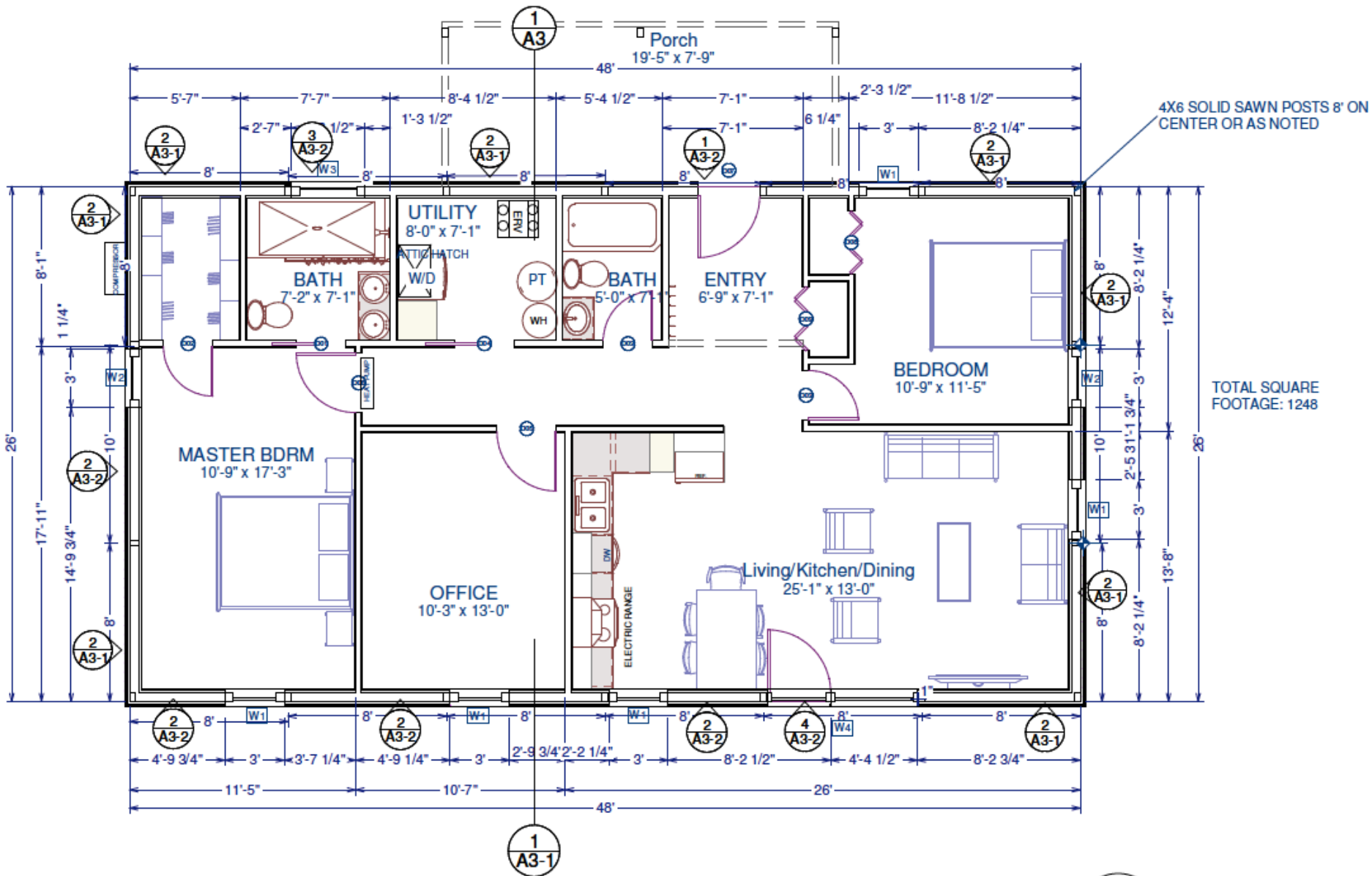
REFERENCE MAP: "WOODLAND ACRES SUBDIVISION", FILED IN THE ORANGE COUNTY CLERK'S OFFICE ON JUNE 21, 1978, AS MAP #4545.
 CONTOURS AND ELEVATIONS SHOWN ARE FROM AN ACTUAL FIELD SURVEY PERFORMED ON JULY 16, 2013. DATUM FOR SAID SURVEY IS APPROXIMATE U.S.G.S.
 PARCEL CONTAINS 1.83 ACRES, MORE OR LESS.

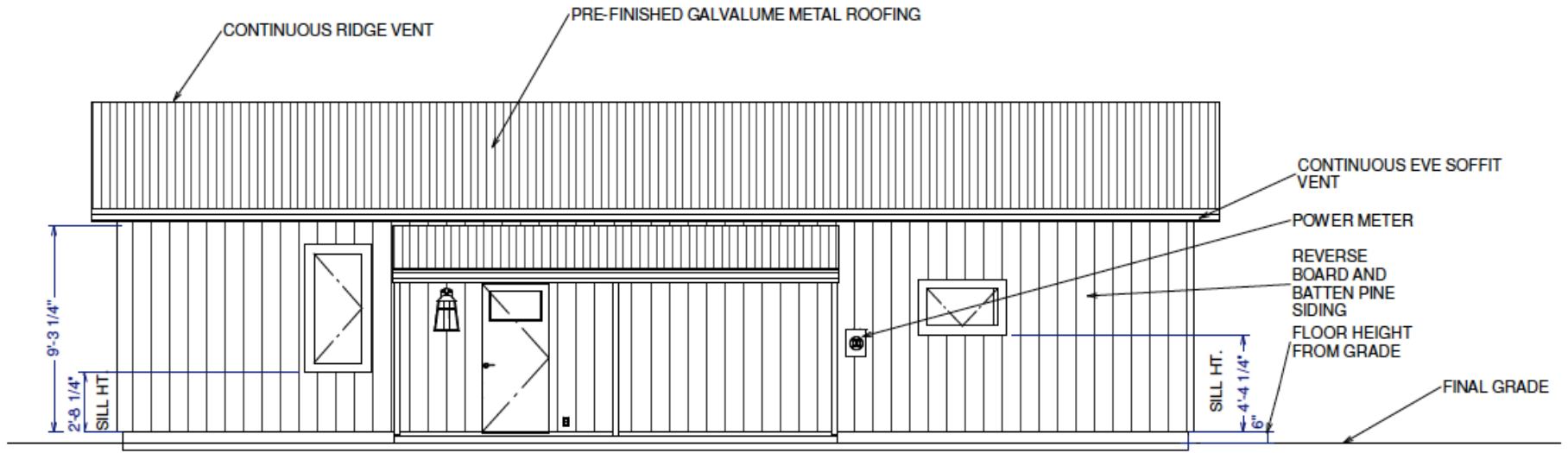
LEGEND

-  UTILITY POLE
-  CONTOUR LINE AND ELEVATION
-  PERGOLATION TEST
-  TEST PIT/ SOIL PROBE
-  NOW OR FORMERLY



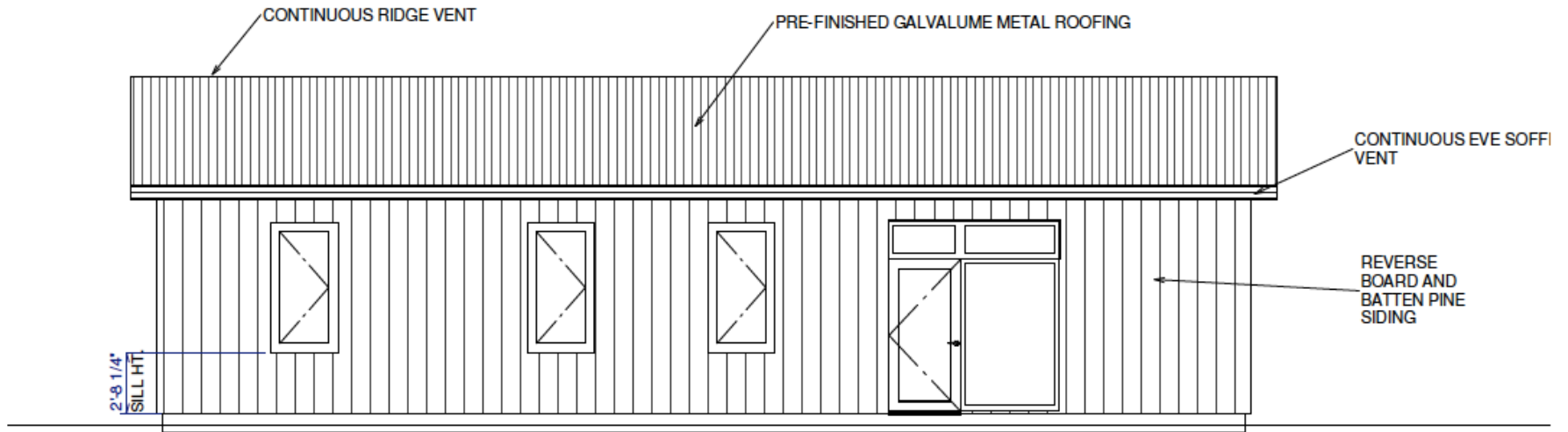






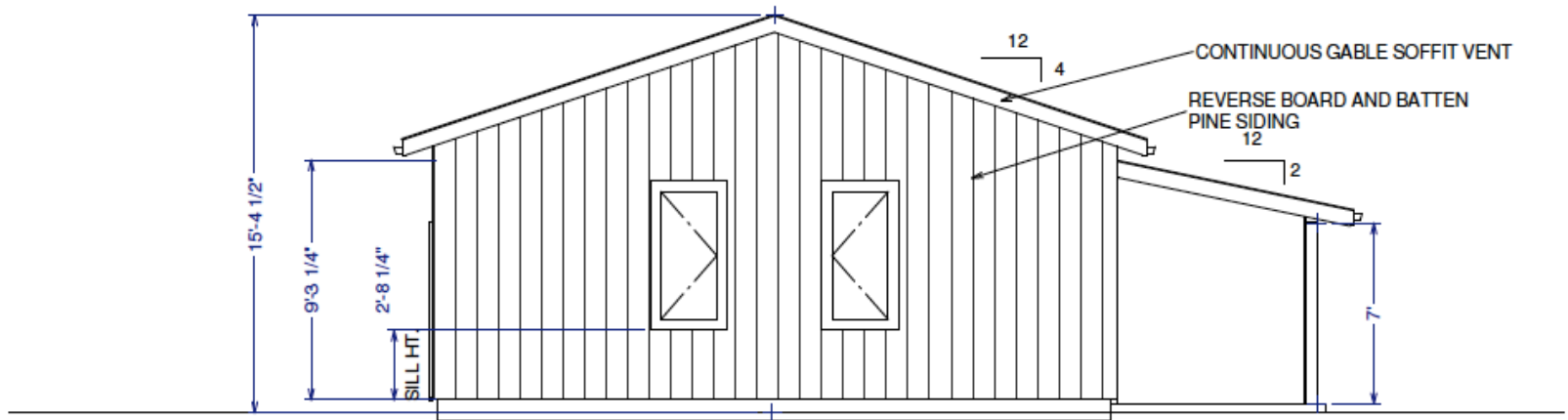
1 NORTH ELEVATION
A4-1 SCALE: 3/16" = 1'

N glazing 1.3% of GFA



2 SOUTH ELEVATION
A4-1 SCALE: 3/16" = 1'

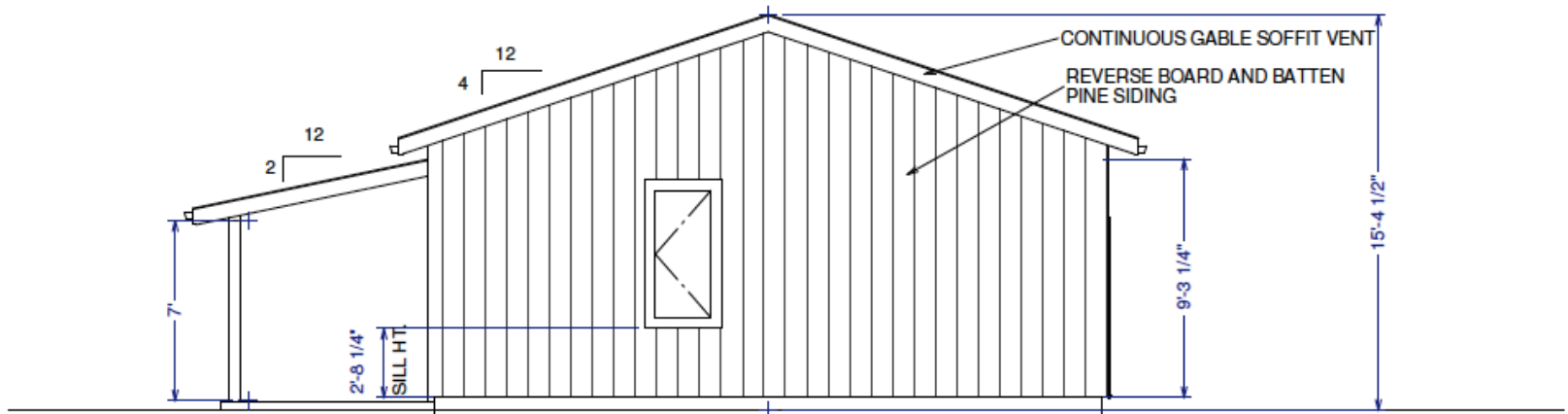
S glazing 6.3% of GFA



1
A4-2

EAST ELEVATION
SCALE: 3/16" = 1'

E glazing 1.7% of GFA

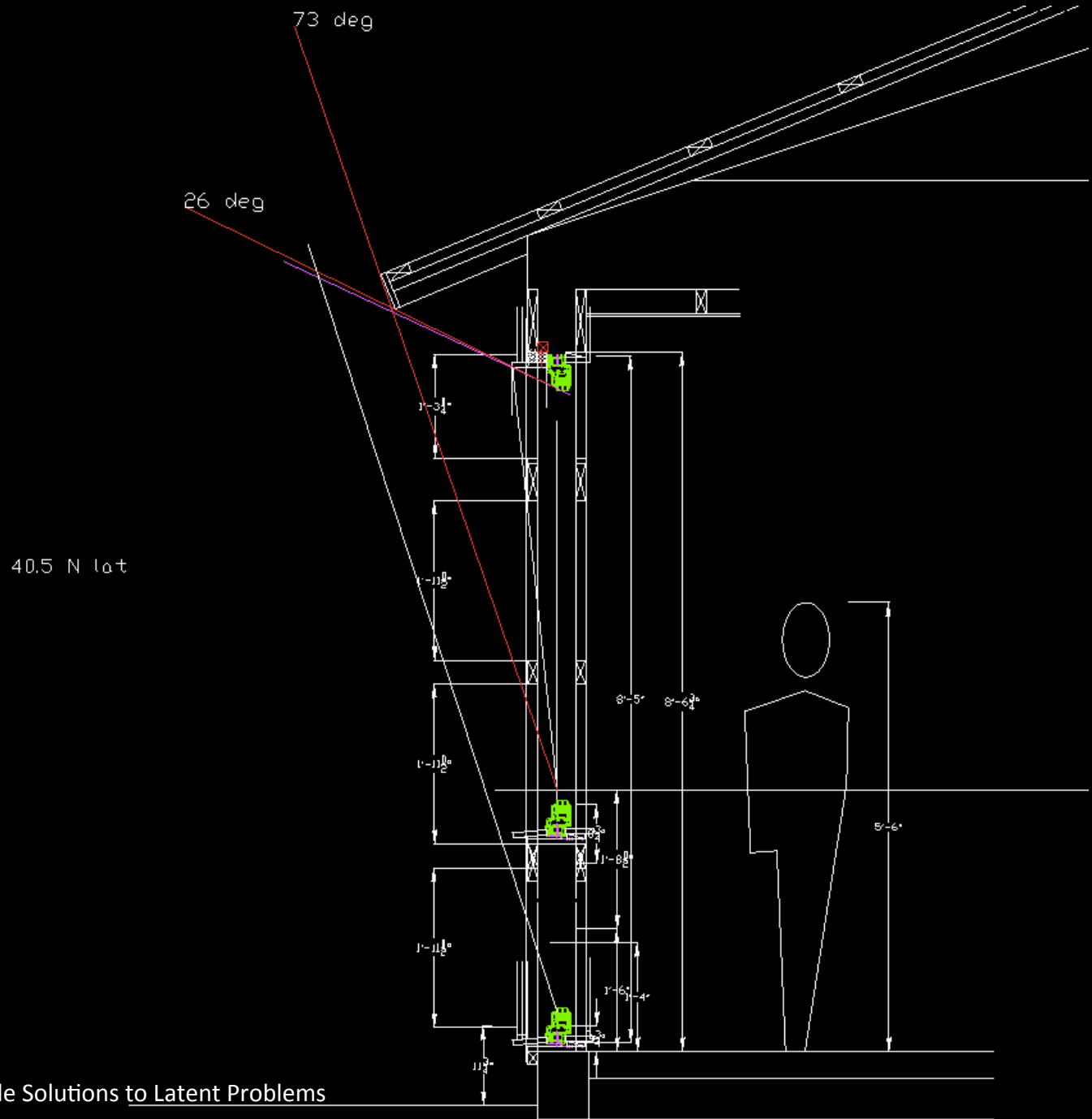


2
A4-2

WEST ELEVATION
SCALE: 3/16" = 1'

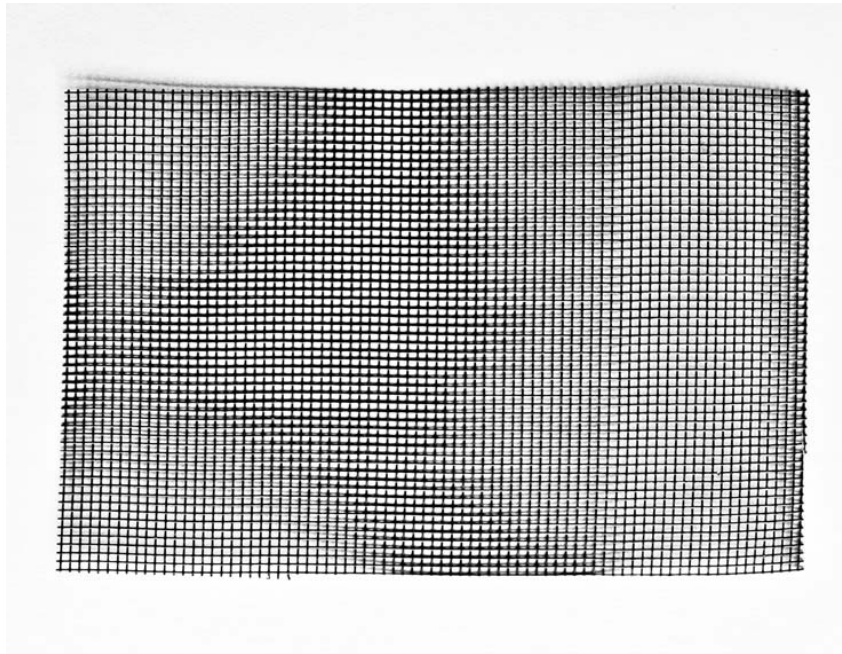
W glazing 0.9% of GFA

Total glazing 10% of GFA



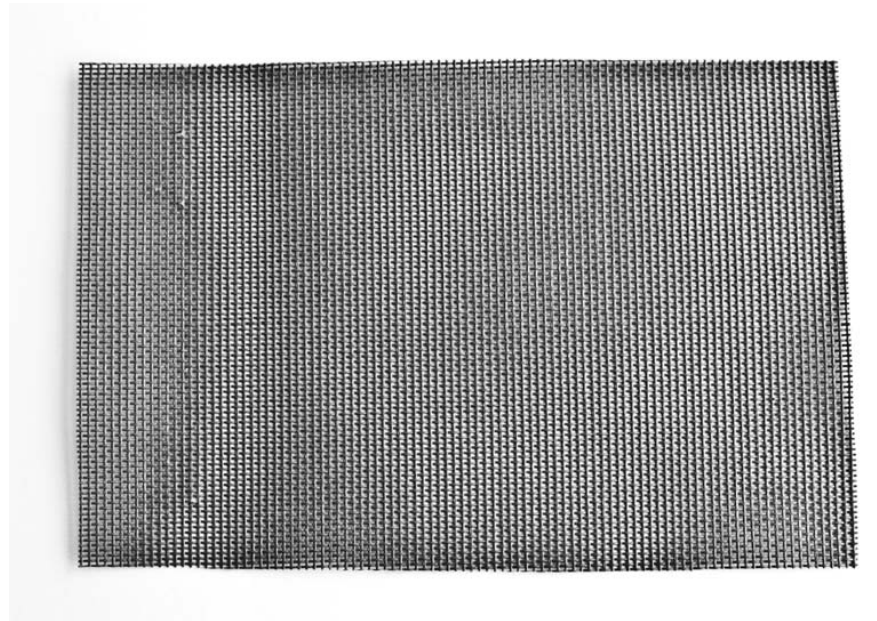
STANDARD MESH

SHGC reduction factor 33%



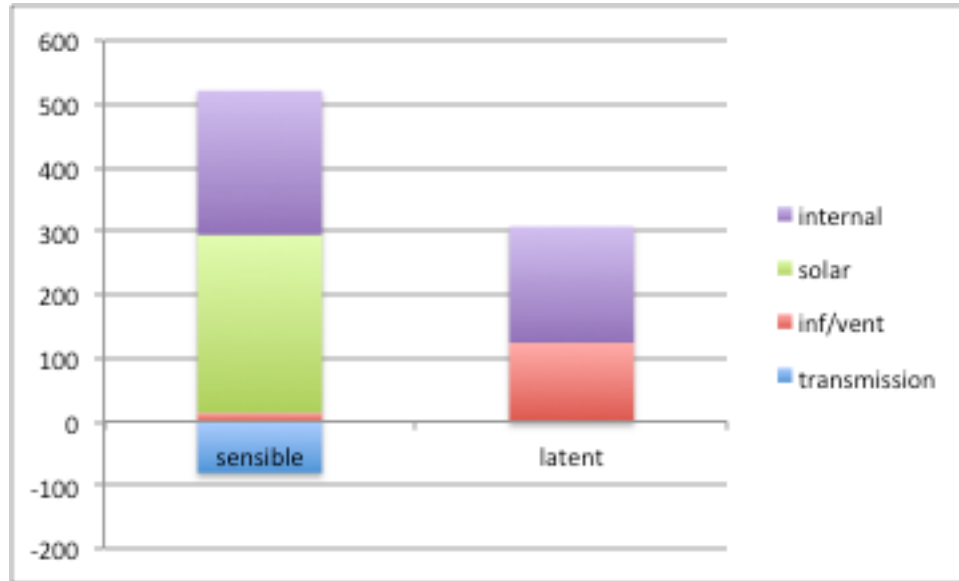
THERMO MESH

SHGC reduction factor 64%



Base Case

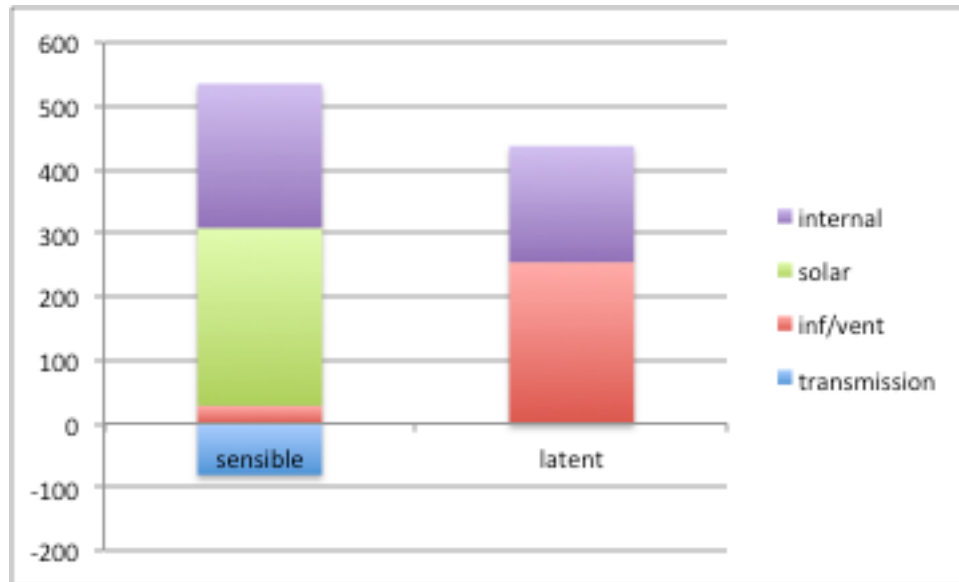
SHF = 0.59



42 cfm vent, 0.5 ach50, 0.5 SHGC glass

Leaky House

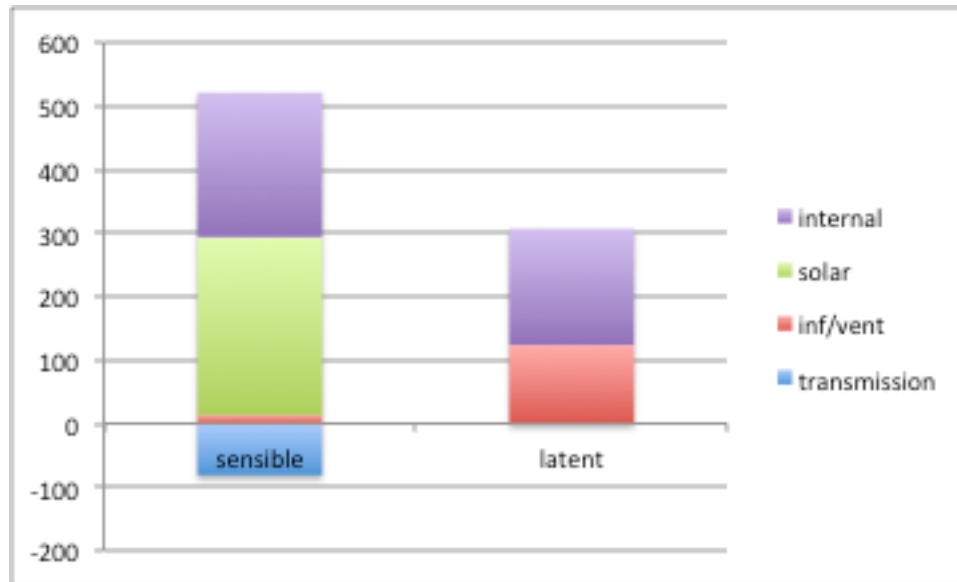
SHF = 0.51



2 ach50

Base Case

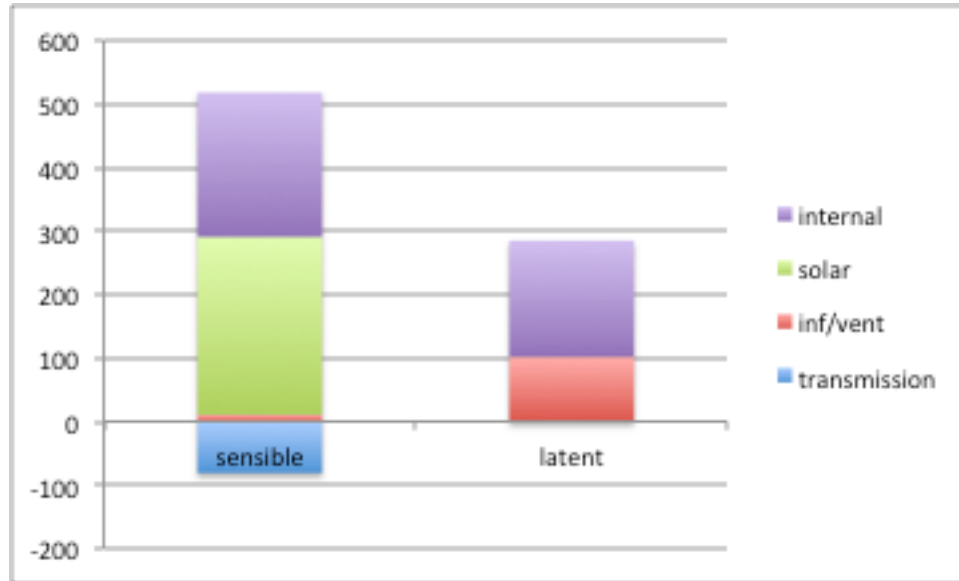
SHF = 0.59



42 cfm vent, 0.5 ach50, 0.5 SHGC glass, 77%/62% ERV

Crazy Tight House

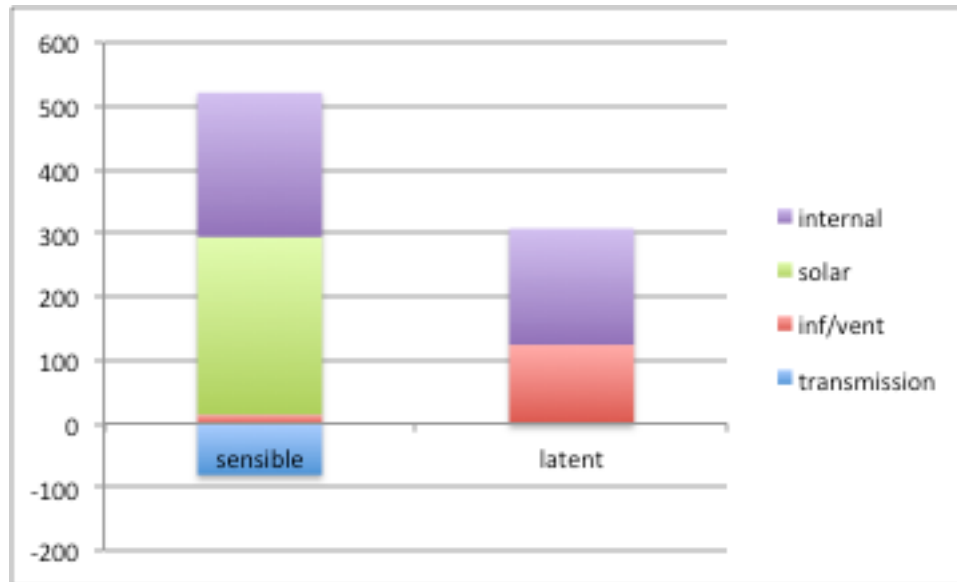
SHF = 0.61



0.25 ach50

Base Case

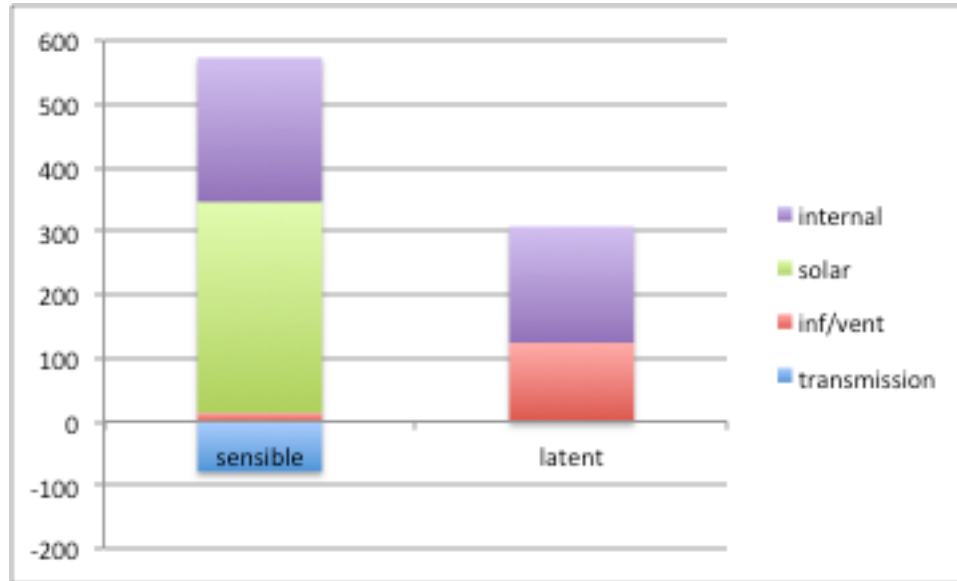
SHF = 0.59



42 cfm vent, 0.5 ach50, 0.5 SHGC glass, 77%/62% ERV

High Gain Glass

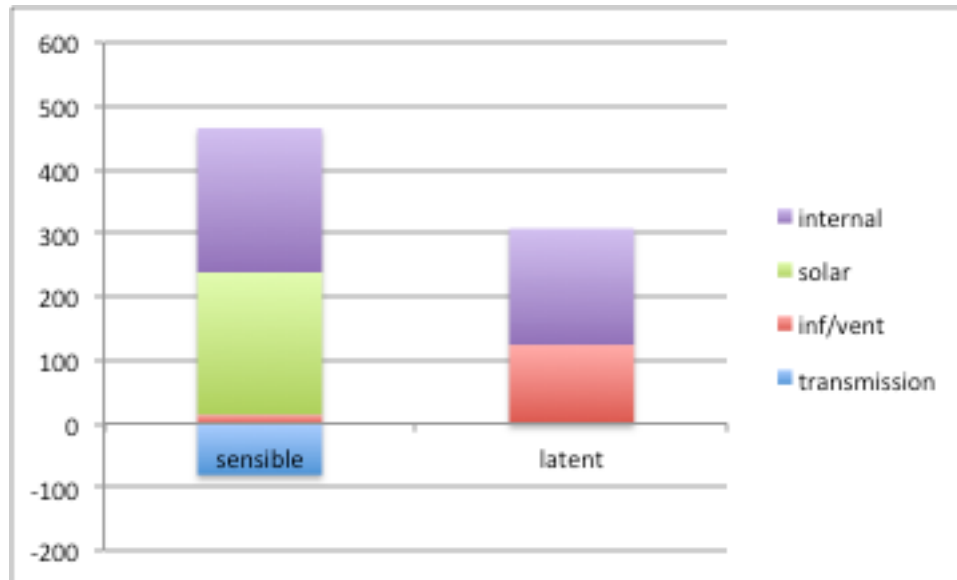
SHF = 0.62



SHGC = 0.62

Low Gain Glass

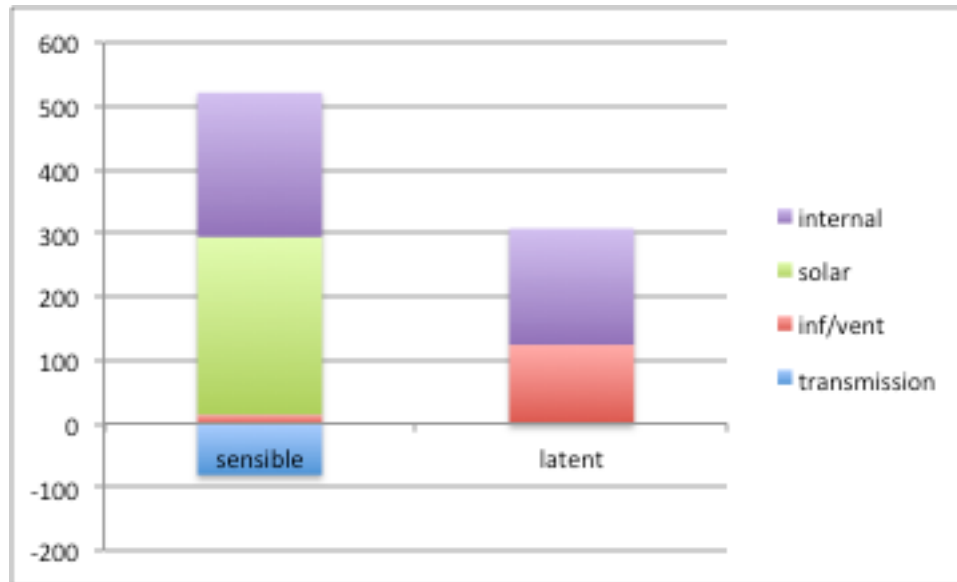
SHF = 0.56



SHGC = 0.37

Base Case

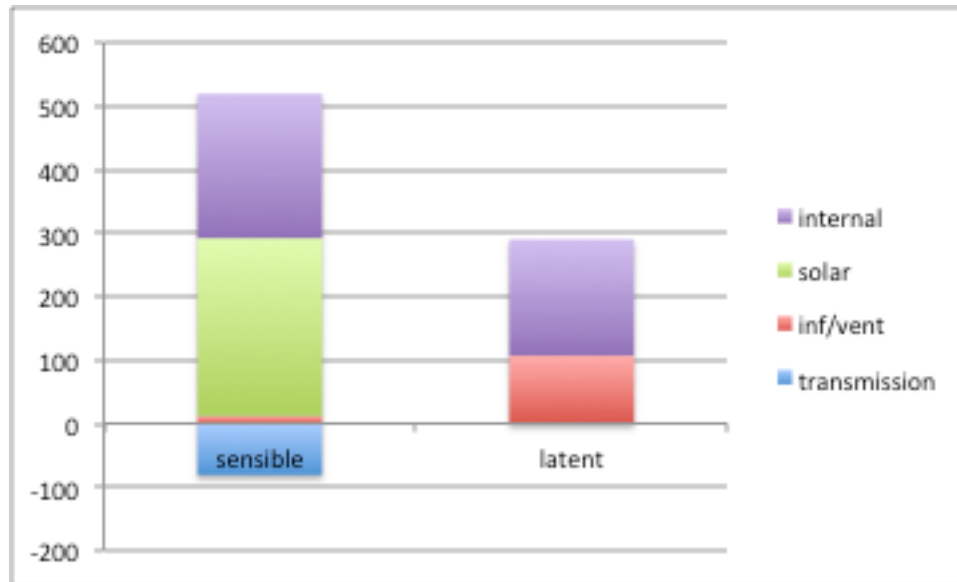
SHF = 0.59



42 cfm vent, 0.5 ach50, 0.5 SHGC glass, 77%/62% ERV

Vent to ASHRAE 62.2-2010

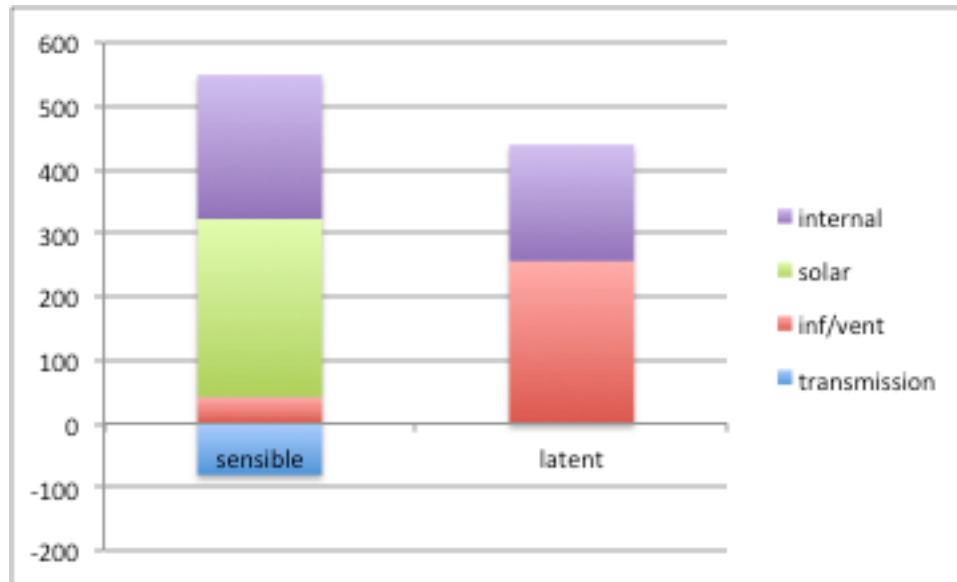
SHF = 0.60



35 cfm ventilation

Vent to ASHRAE 62.2-2013

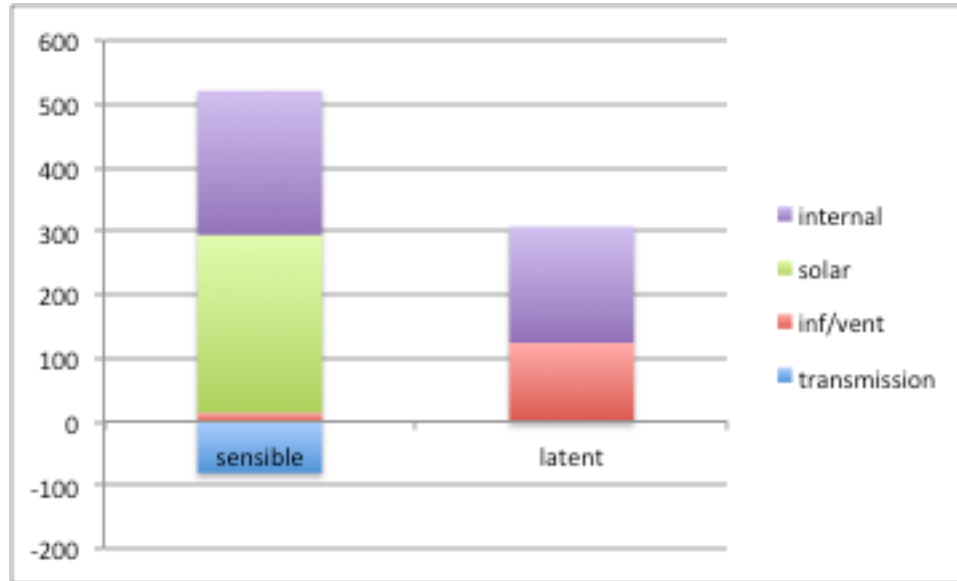
SHF = 0.57



60 cfm ventilation

Base Case

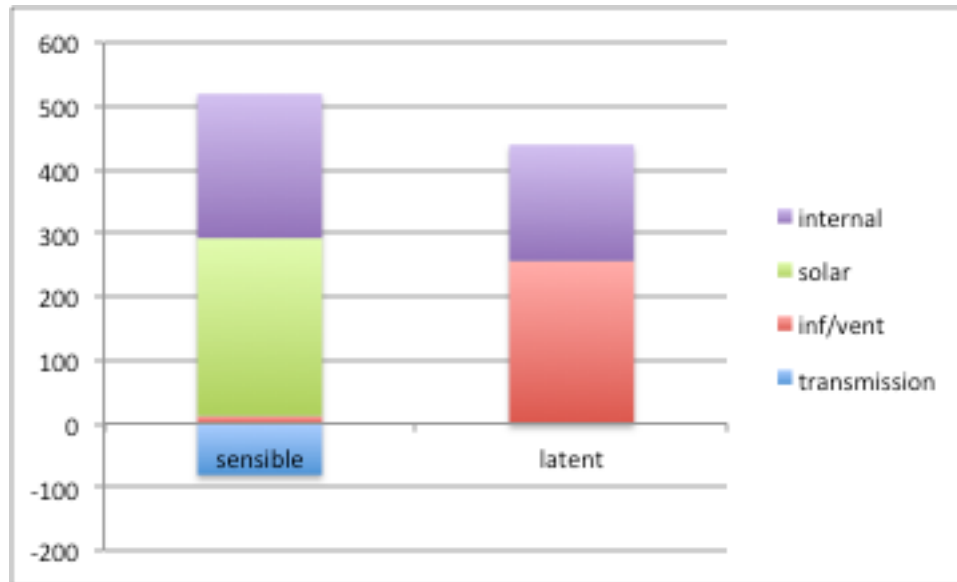
SHF = 0.59



42 cfm vent, 0.5 ach50, 0.5 SHGC glass, 77%/62% ERV

HRV

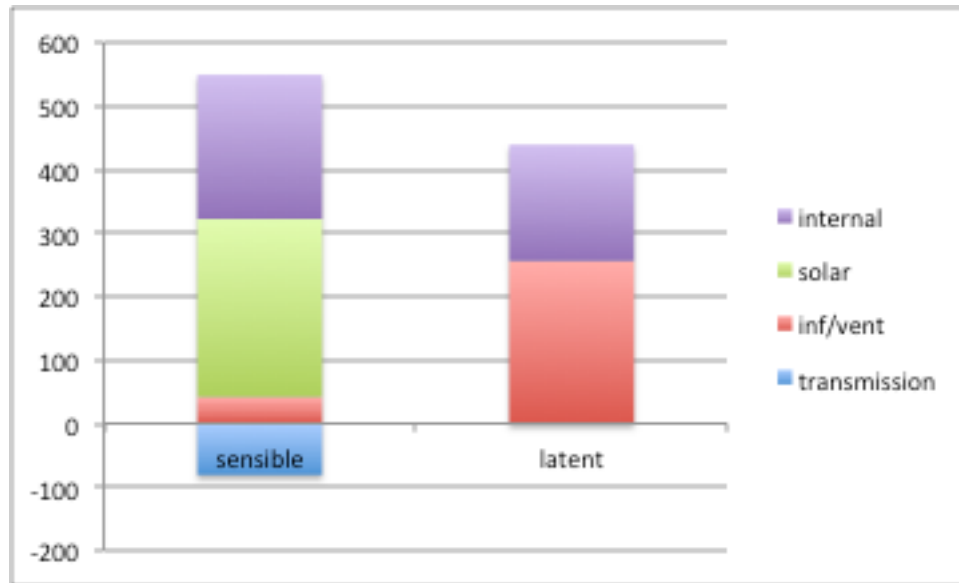
SHF = 0.50



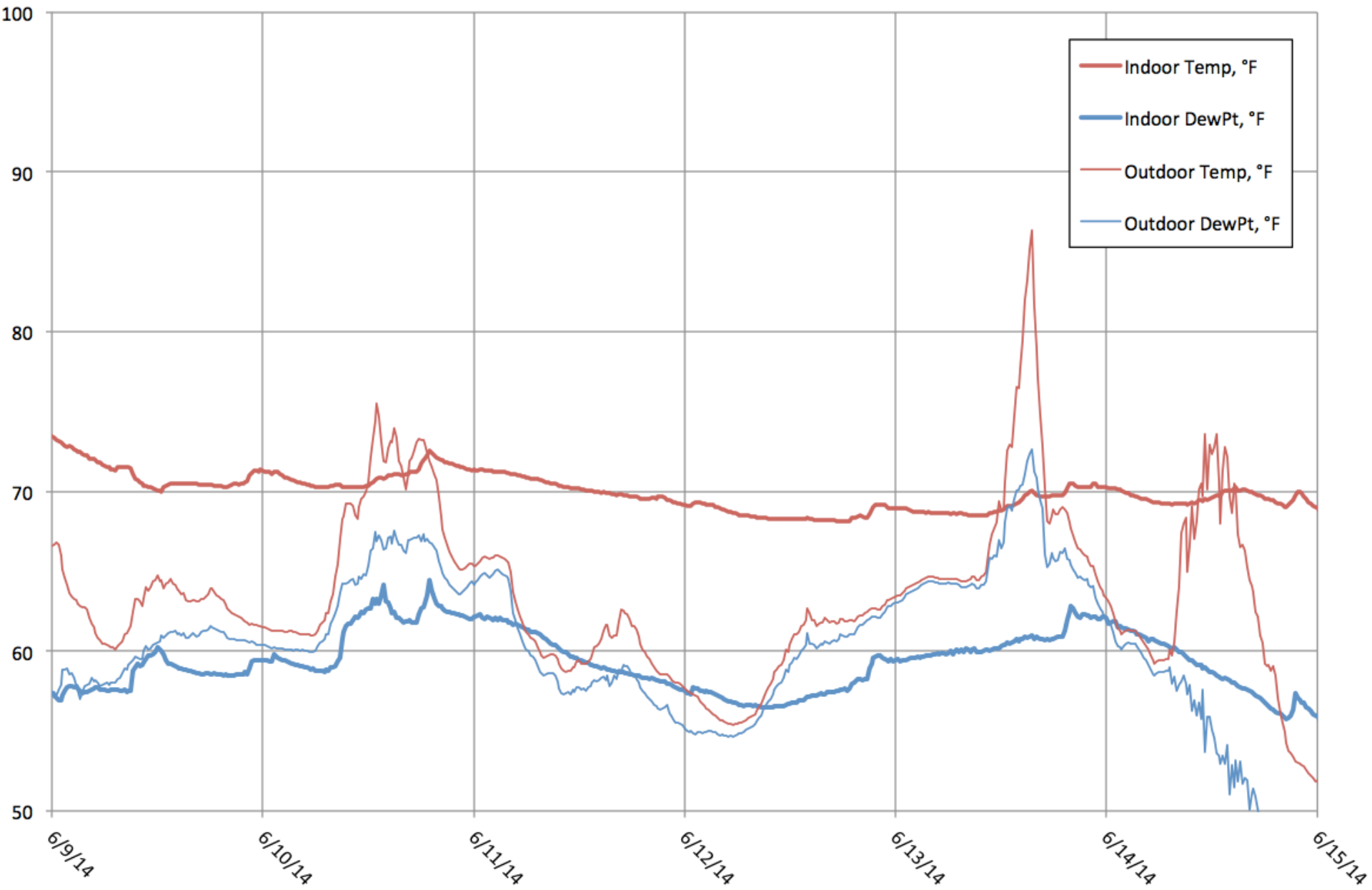
Eff = 84%

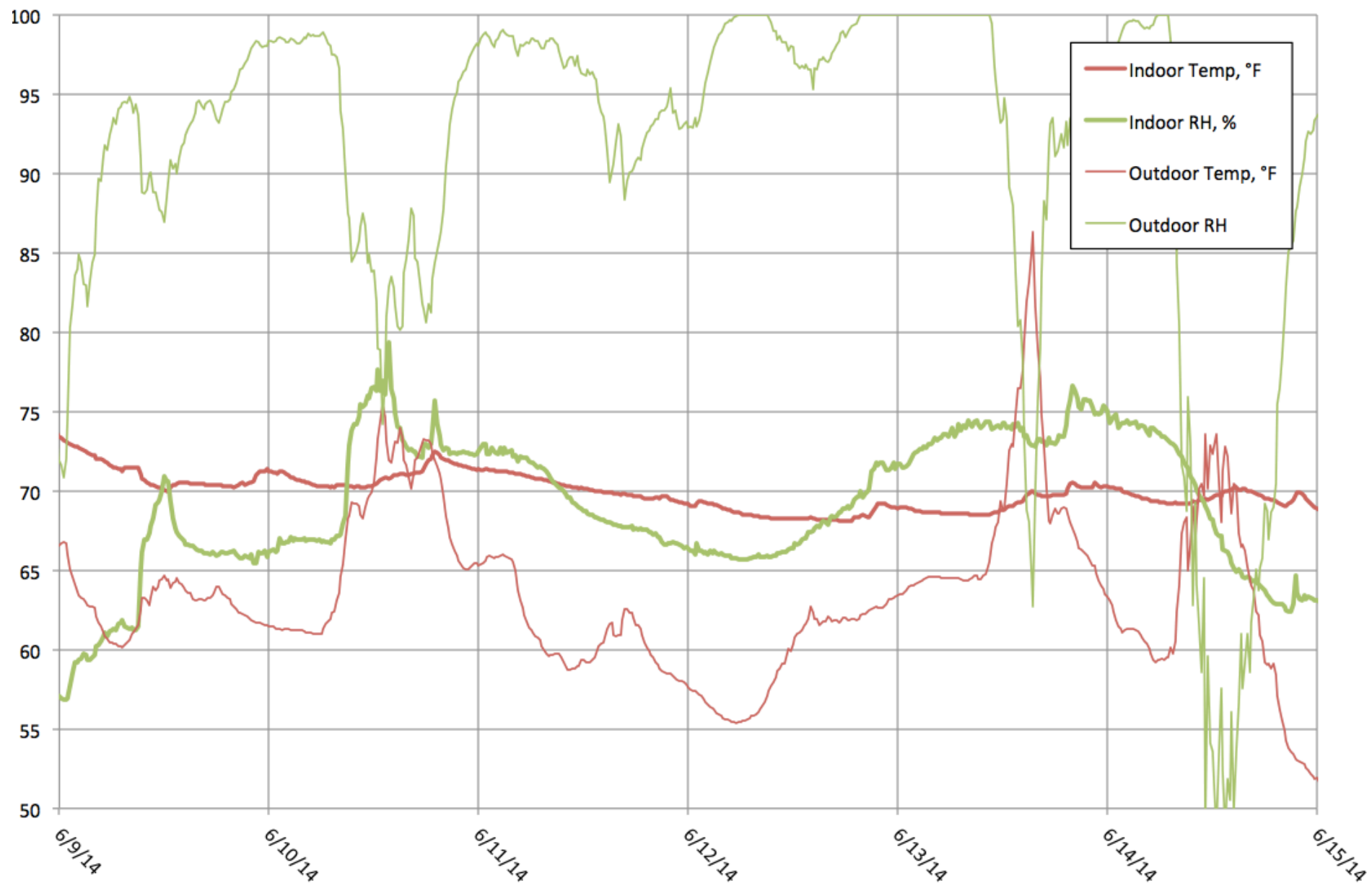
No HRV or ERV (as operated)

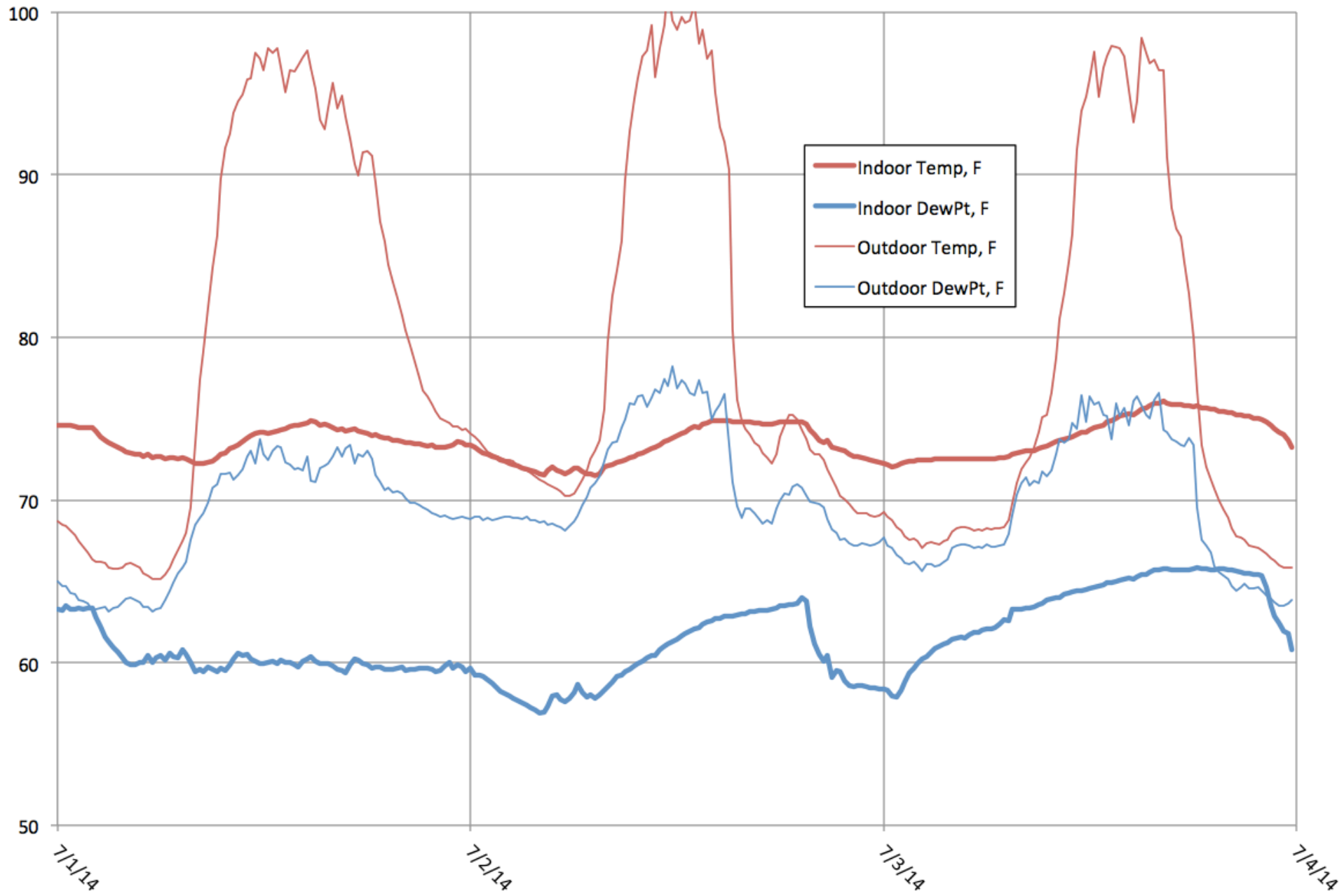
SHF = 0.52

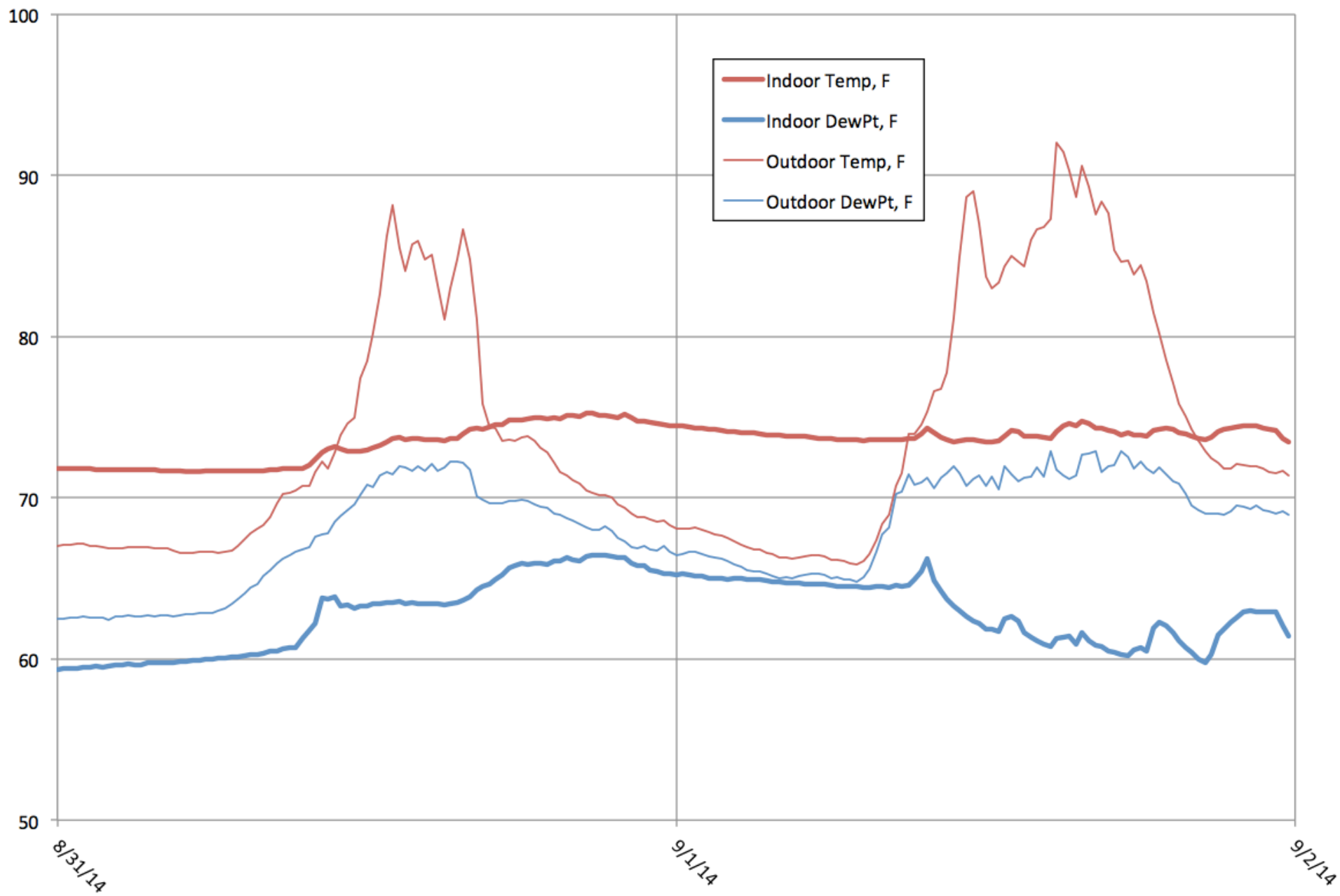












Conclusions

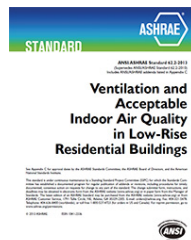
- Humidity can probably be controlled in above-grade, low-load homes in the Northeast without the need for a dehumidifier
- Climate may become more humid in coming decades

Ventilation: How much air do we need?

Depends upon who you ask...



International Mechanical Code (IMC) 2012

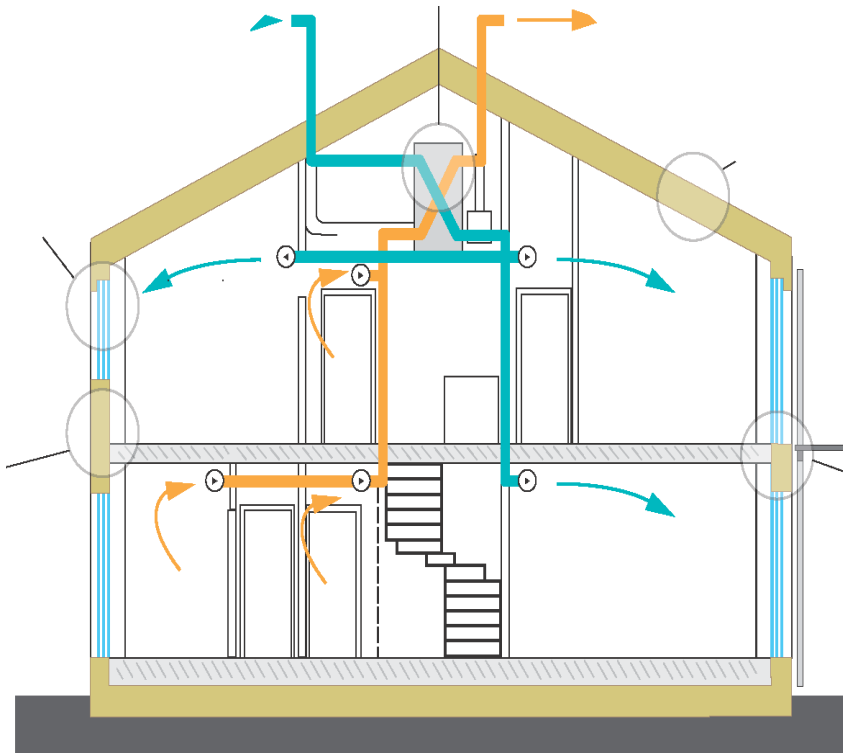


ASHRAE Standard 62.2
Ventilation and Acceptable Indoor Air Quality
in Low-Rise Residential Buildings
2010 Version and 2013 Version



Passive House Institute (PHI)

Example House for Ventilation



2,600 SF (2,400 TFA for PHI)
8 FT Ceilings
4 bedrooms
2-1/2 Bathrooms

IMC 2012 Airflow

Referenced by the International Residential Code (IRC)
Adopted by all Northeast states except Vermont



0.35 Air Changes per Hour (ACH)

- But not less than 15 CFM per person

Kitchen exhaust: 25 CFM continuous

Bathroom exhaust: 20 CFM continuous

Toilet room exhaust: 20 CFM continuous

$2600\text{SF} * 8\text{FT} = 20,800 \text{ CF}$ at 0.35 ACH

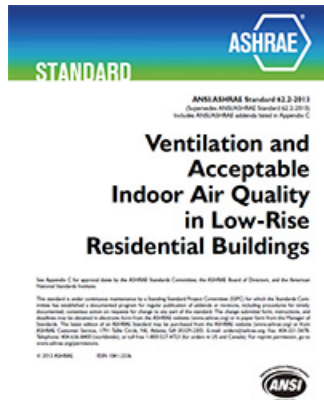
121 CFM

Kitchen + 2 Bathrooms + Toilet Room

85 CFM

ASHRAE Standard 62.2-2010 Airflow

Referenced by LEED for Homes, EnergyStar, Mass Tier III Program
Tends to lead the IMC



7.5 CFM per person (number of bedrooms +1)
AND 0.01 CFM/SF

Kitchen exhaust: 5 ACH continuous (!)
or 100 CFM intermittent hood

Bathroom exhaust: 20 CFM continuous

Bathroom: Any room containing a bathtub, a shower, a spa, or similar source of moisture

$7.5(4+1) + 0.01(2600) =$

64 CFM

2 Bathrooms (+ Toilet Room)

40 CFM (60 CFM)

If assume a modest 150 SF Kitchen

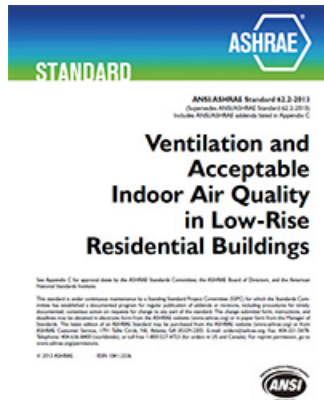
100 CFM !

- Best to include an intermittent range hood.

ASHRAE Standard 62.2-2013 Airflow

Option for Mass Tier III

Controversial new version of 62.2



7.5 CFM per person (number of bedrooms +1)

AND **0.03** CFM/SF

Kitchen exhaust: 5 ACH continuous (!)

or 100 CFM intermittent hood

Bathroom exhaust: 20 CFM continuous

Bathroom: Any room containing a bathtub, a shower, a spa, or similar source of moisture

$7.5(4+1) + 0.03(2600) =$

2 Bathrooms (+ Toilet Room)

Likely range hood for Kitchen

116 CFM

40 CFM (60 CFM)

Passive House Institute Airflow

Airflows required for a certifying Passive House project



0.30 Air Changes per Hour (ACH) of TFA

Kitchen exhaust: 35 CFM continuous

Bathroom exhaust: 24 CFM continuous

Toilet room exhaust: 12 CFM continuous

Laundry room exhaust: 12 CFM continuous

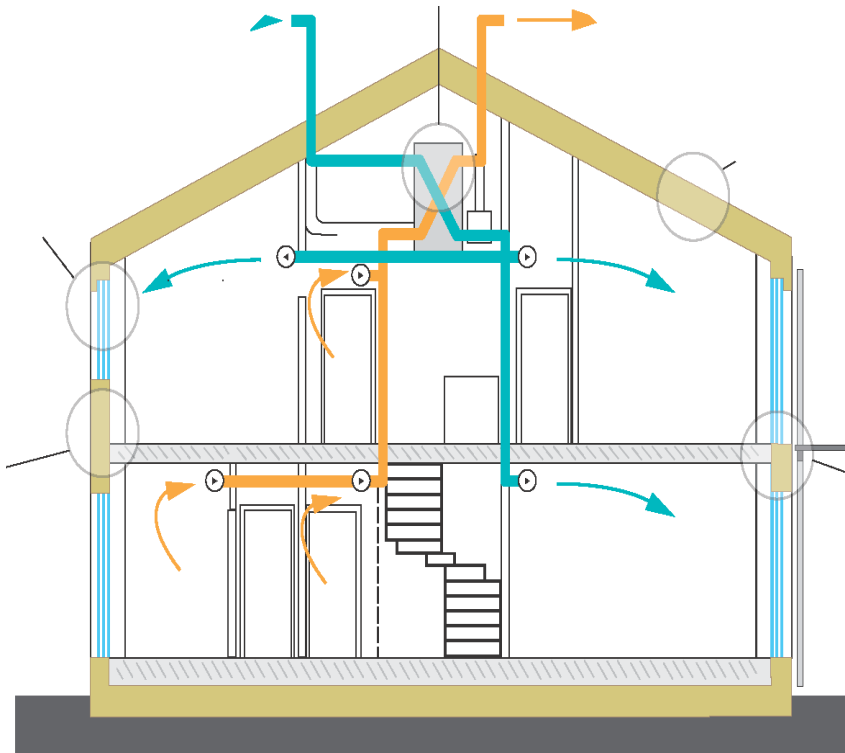
2400SF * 8FT = 19,200 CF at 0.30 ACH

96 CFM

Kitchen + 2 Bathrooms + Toilet Room

95 CFM

Example House for Ventilation



2,600 SF (2,400 TFA for PHI)
 8 FT Ceilings
 4 bedrooms
 2-1/2 Bathrooms

Standard	Supply	Exhaust
IMC	121 CFM	85 CFM
62.2-2010	63 CFM	60 CFM*
62.2-2013	116 CFM	60 CFM*
PHI	96 CFM	95 CFM

* With Intermittent range hood

Design Conditions: Cooling

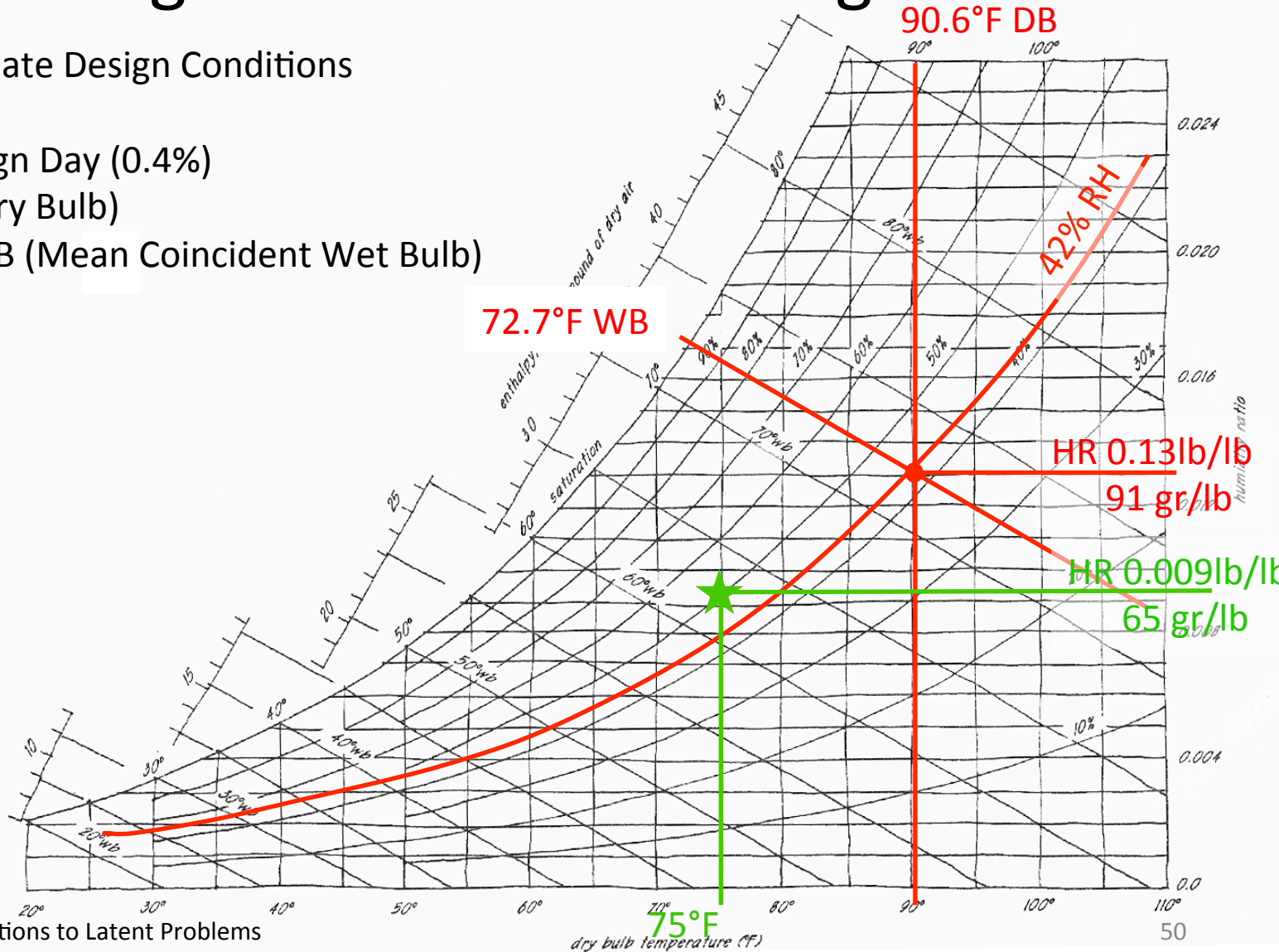
ASHRAE Climate Design Conditions

Boston, MA

Cooling Design Day (0.4%)

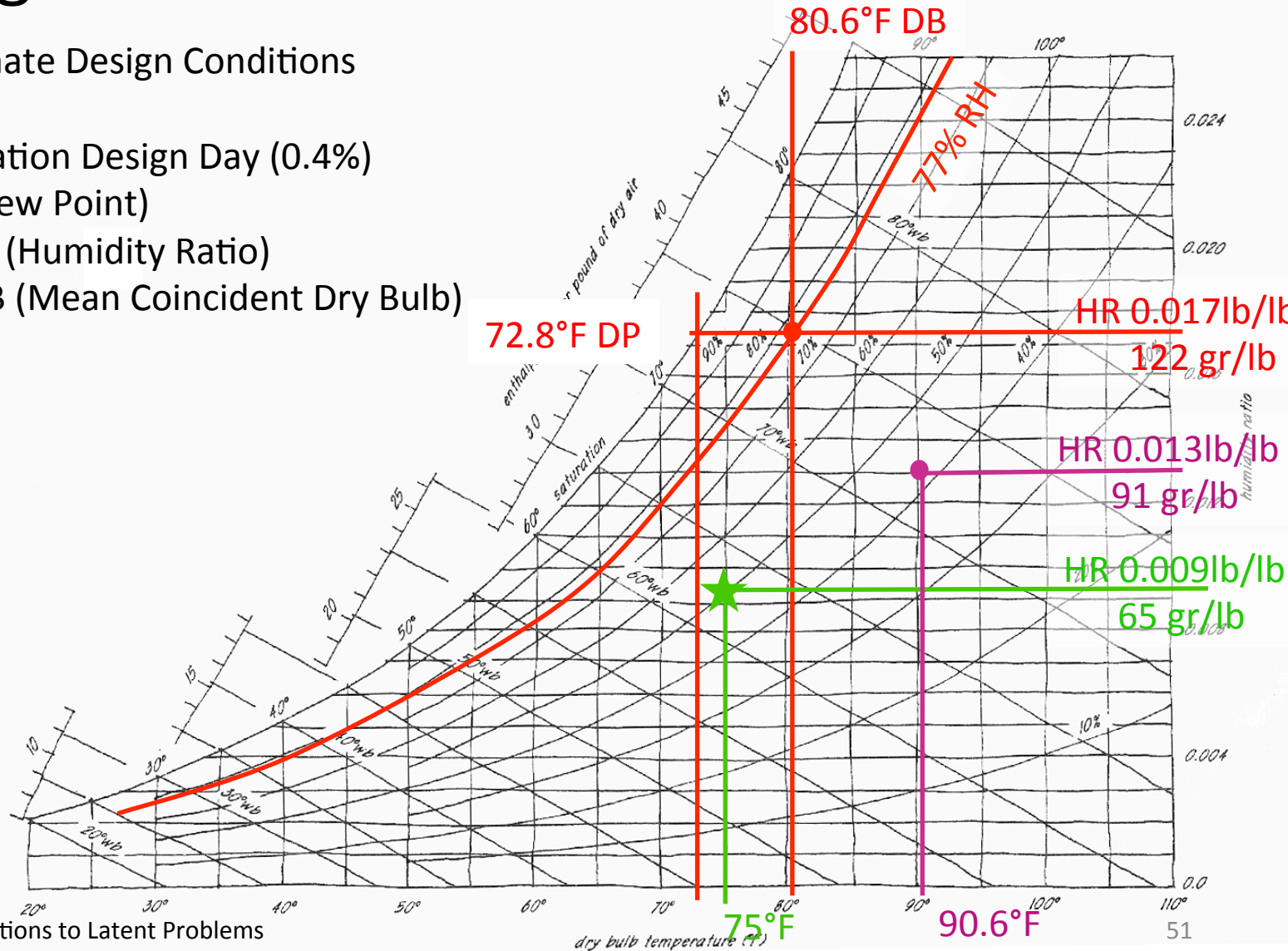
90.6°F DB (Dry Bulb)

72.7°F MCWB (Mean Coincident Wet Bulb)



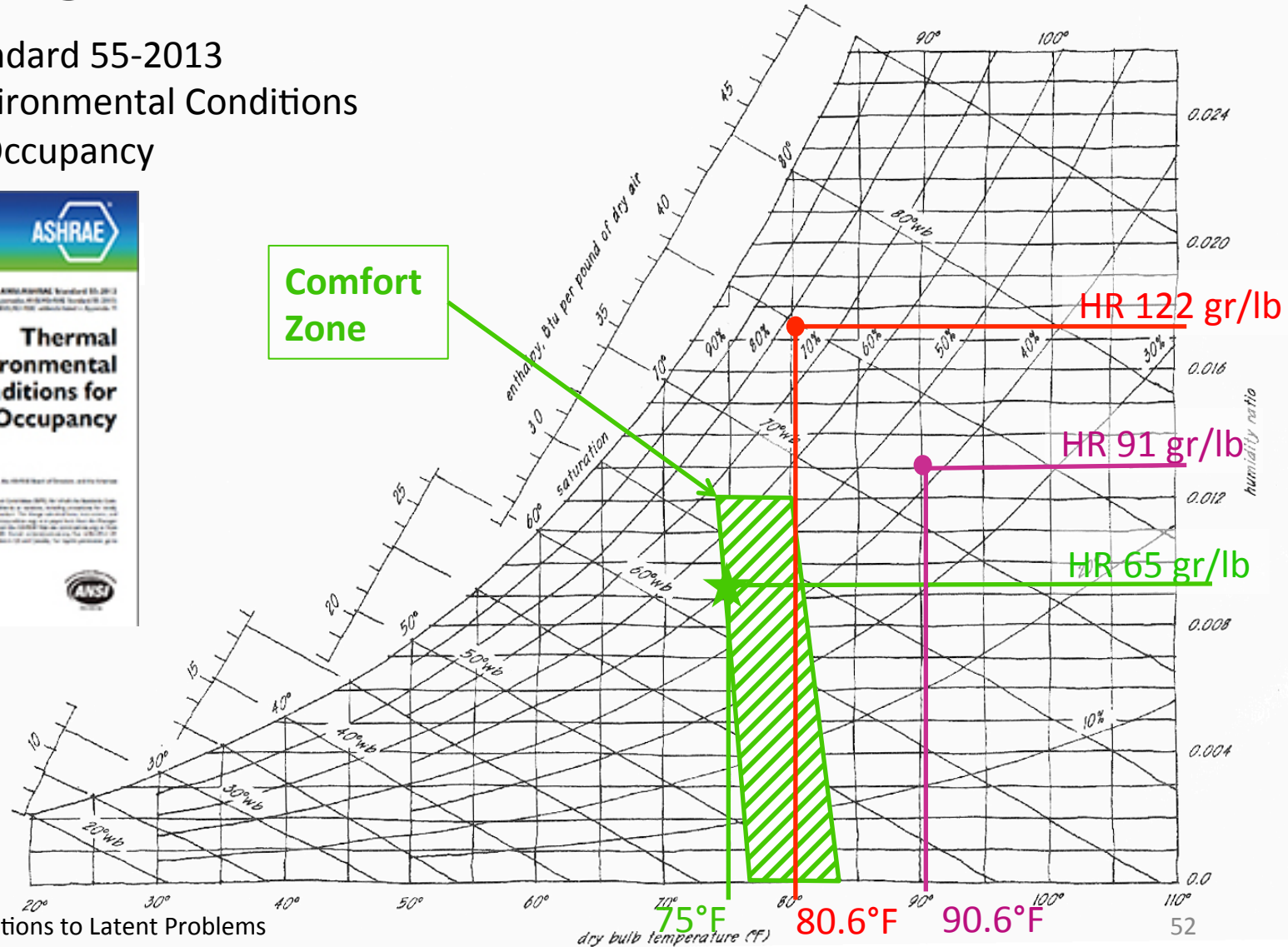
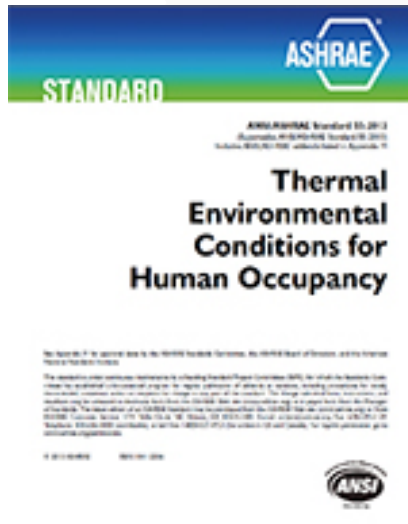
Design Conditions: Dehumidification

ASHRAE Climate Design Conditions
Boston
Dehumidification Design Day (0.4%)
72.8°F DP (Dew Point)
122 gr/lb HR (Humidity Ratio)
80.6°F MCDB (Mean Coincident Dry Bulb)



Design Conditions: Comfort Zone

ASHRAE Standard 55-2013
Thermal Environmental Conditions
for Human Occupancy



Ventilation loads: Cooling Design Day

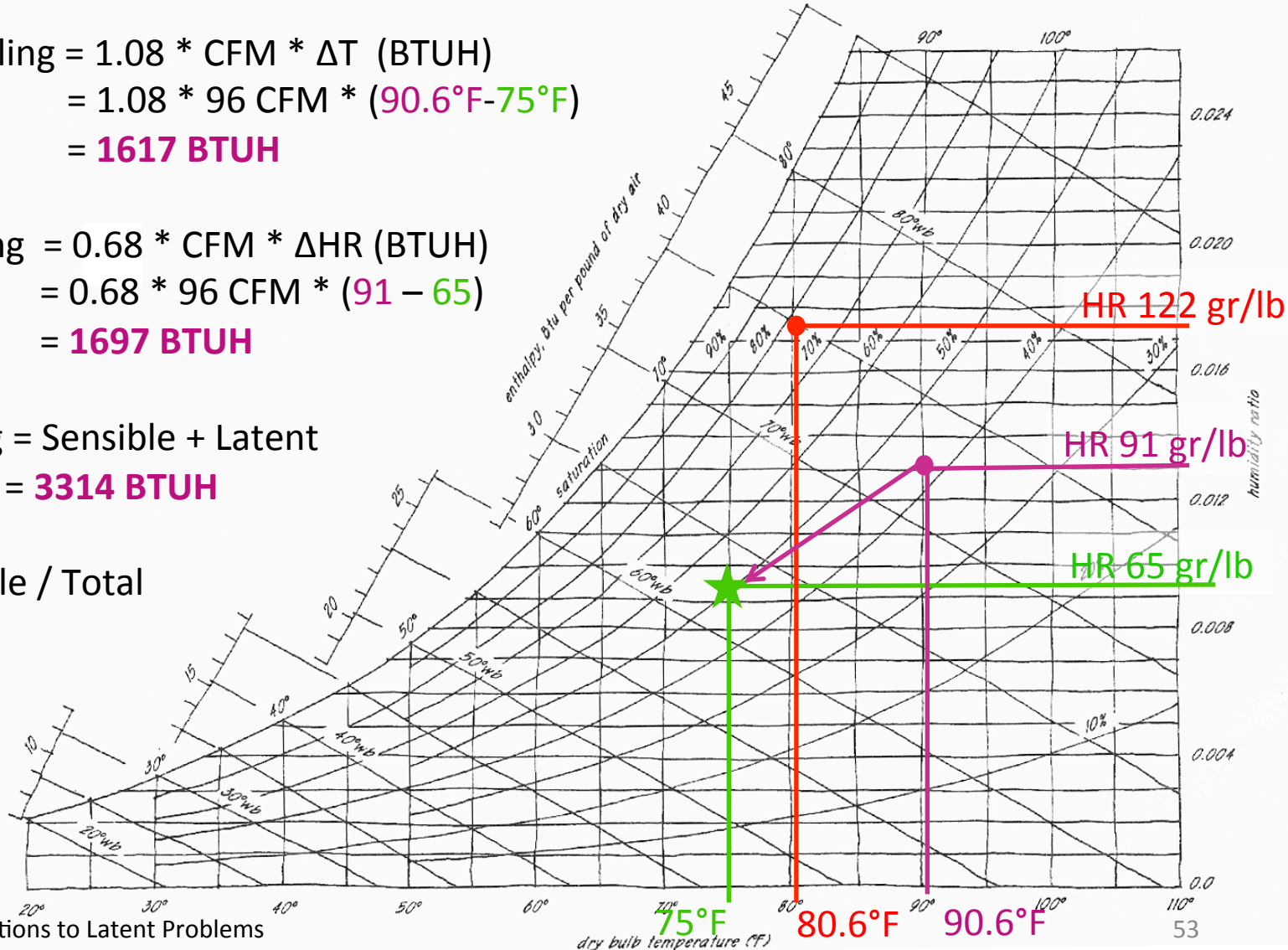
$$\begin{aligned} \text{Sensible Cooling} &= 1.08 * \text{CFM} * \Delta T \text{ (BTUH)} \\ &= 1.08 * 96 \text{ CFM} * (90.6^\circ\text{F} - 75^\circ\text{F}) \\ &= \mathbf{1617 \text{ BTUH}} \end{aligned}$$

$$\begin{aligned} \text{Latent Cooling} &= 0.68 * \text{CFM} * \Delta \text{HR (BTUH)} \\ &= 0.68 * 96 \text{ CFM} * (91 - 65) \\ &= \mathbf{1697 \text{ BTUH}} \end{aligned}$$

$$\begin{aligned} \text{Total Cooling} &= \text{Sensible} + \text{Latent} \\ &= \mathbf{3314 \text{ BTUH}} \end{aligned}$$

$$\text{SHR} = \text{Sensible} / \text{Total}$$

$$\text{SHR} = 0.48$$



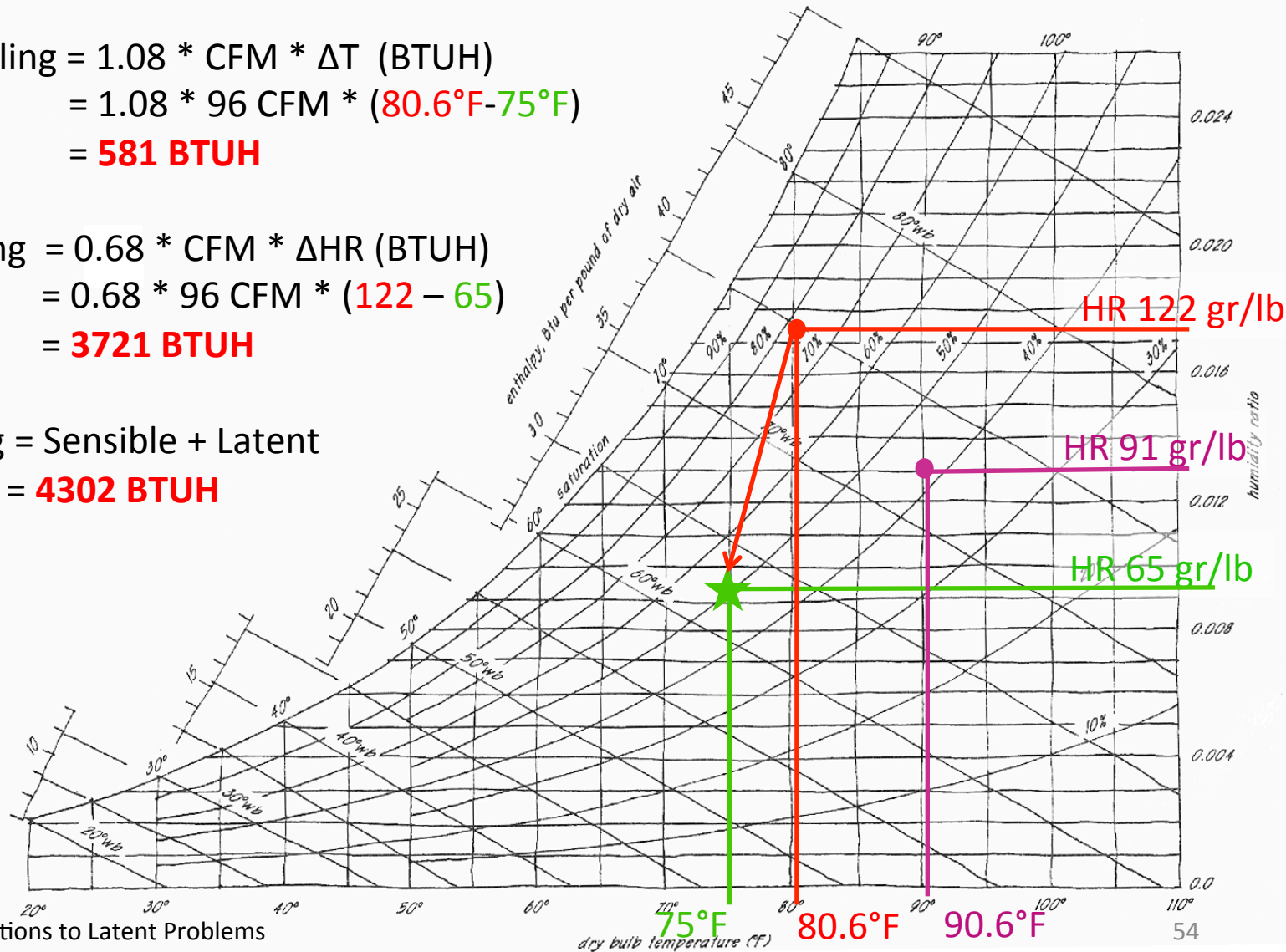
Ventilation loads: Dehumidification Design Day

$$\begin{aligned} \text{Sensible Cooling} &= 1.08 * \text{CFM} * \Delta T \text{ (BTUH)} \\ &= 1.08 * 96 \text{ CFM} * (80.6^\circ\text{F} - 75^\circ\text{F}) \\ &= \mathbf{581 \text{ BTUH}} \end{aligned}$$

$$\begin{aligned} \text{Latent Cooling} &= 0.68 * \text{CFM} * \Delta \text{HR (BTUH)} \\ &= 0.68 * 96 \text{ CFM} * (122 - 65) \\ &= \mathbf{3721 \text{ BTUH}} \end{aligned}$$

$$\begin{aligned} \text{Total Cooling} &= \text{Sensible} + \text{Latent} \\ &= \mathbf{4302 \text{ BTUH}} \end{aligned}$$

SHR = 0.13

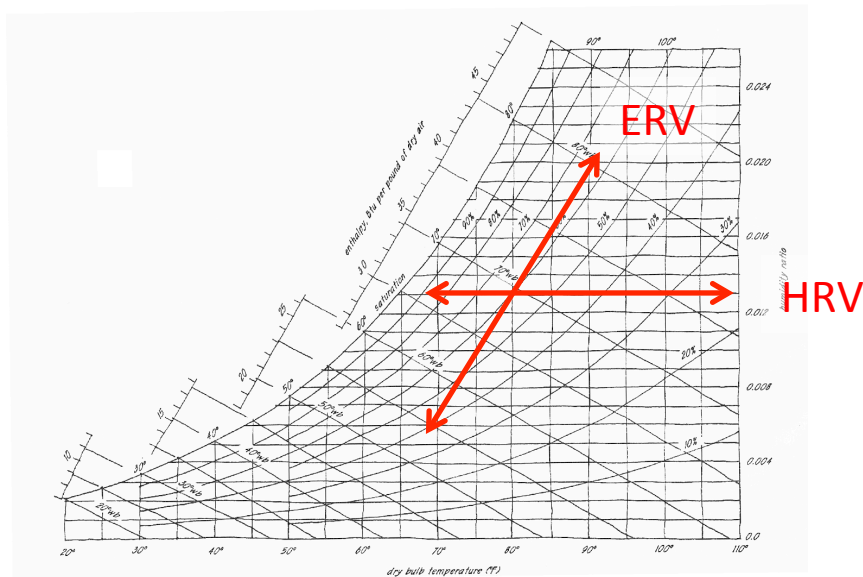


Energy Recovery Ventilation

Two Main Types: HRVs and ERVs

HRV: Heat Recovery Ventilator
Transfers sensible energy

ERV: Enthalpy (or Energy) Recovery Ventilator
Transfers sensible and latent energy



Ventilation loads: HRV Effect

Assume a 72% Efficient HRV

Cooling Design Day

Sensible Cooling = $1617 \text{ BTUH} \cdot (1 - 0.72)$
 = **453 BTUH**

Latent Cooling = **1697 BTUH** Unchanged

Total Cooling = **2150 BTUH**

SHR = 0.21 (Was 0.48)
 Recovered 35% Enthalpy

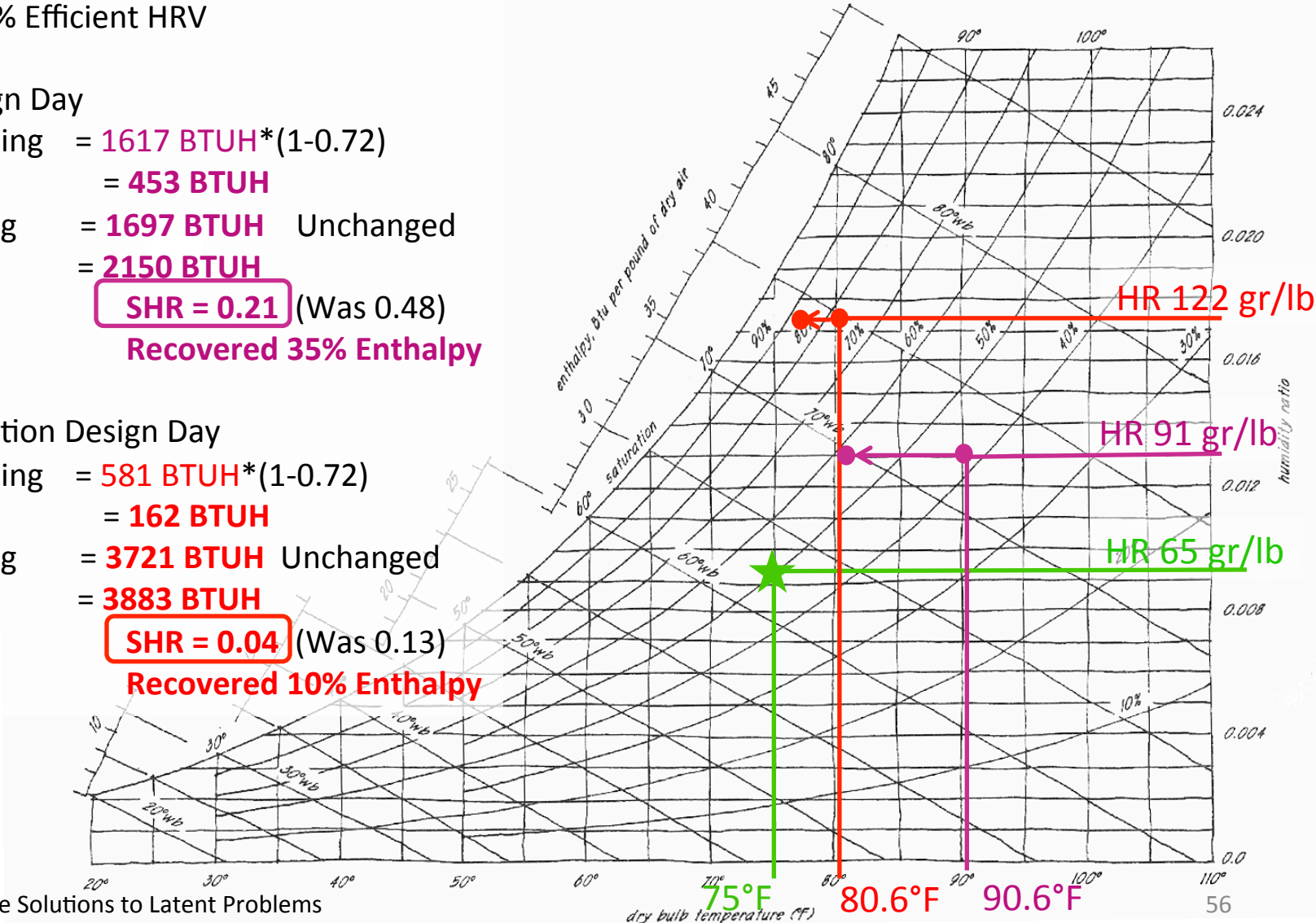
Dehumidification Design Day

Sensible Cooling = $581 \text{ BTUH} \cdot (1 - 0.72)$
 = **162 BTUH**

Latent Cooling = **3721 BTUH** Unchanged

Total Cooling = **3883 BTUH**

SHR = 0.04 (Was 0.13)
 Recovered 10% Enthalpy



Ventilation loads: ERV Effect

Assume a 62% Sensible % 62% Latent Efficient ERV

Cooling Design Day

Sensible Cooling = $1617 \text{ BTUH} \cdot (1-0.62)$
= **615 BTUH**

Latent Cooling = $1697 \text{ BTUH} \cdot (1-0.62)$
= **645 BTUH**

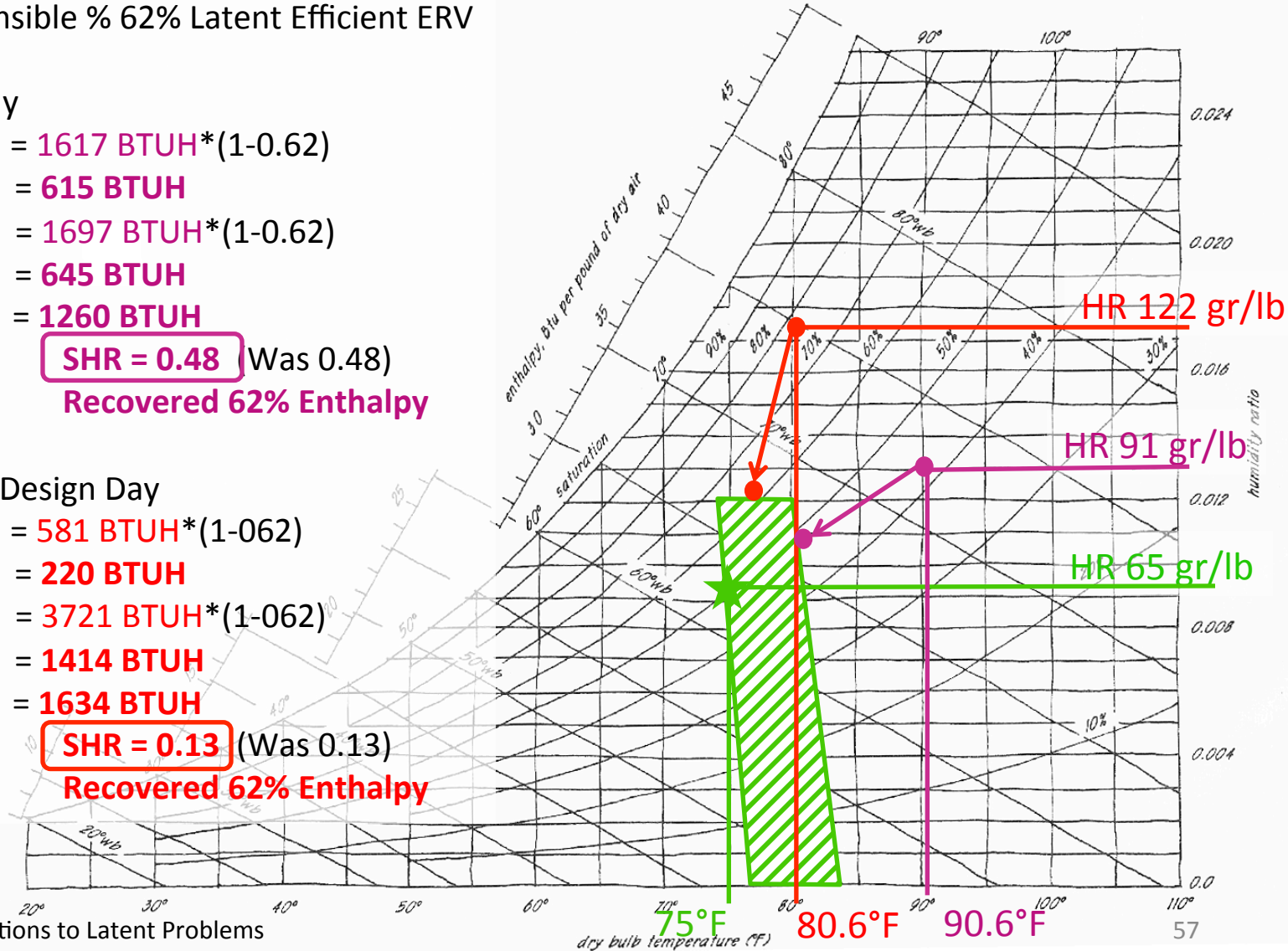
Total Cooling = **1260 BTUH**
SHR = 0.48 (Was 0.48)
Recovered 62% Enthalpy

Dehumidification Design Day

Sensible Cooling = $581 \text{ BTUH} \cdot (1-0.62)$
= **220 BTUH**

Latent Cooling = $3721 \text{ BTUH} \cdot (1-0.62)$
= **1414 BTUH**

Total Cooling = **1634 BTUH**
SHR = 0.13 (Was 0.13)
Recovered 62% Enthalpy



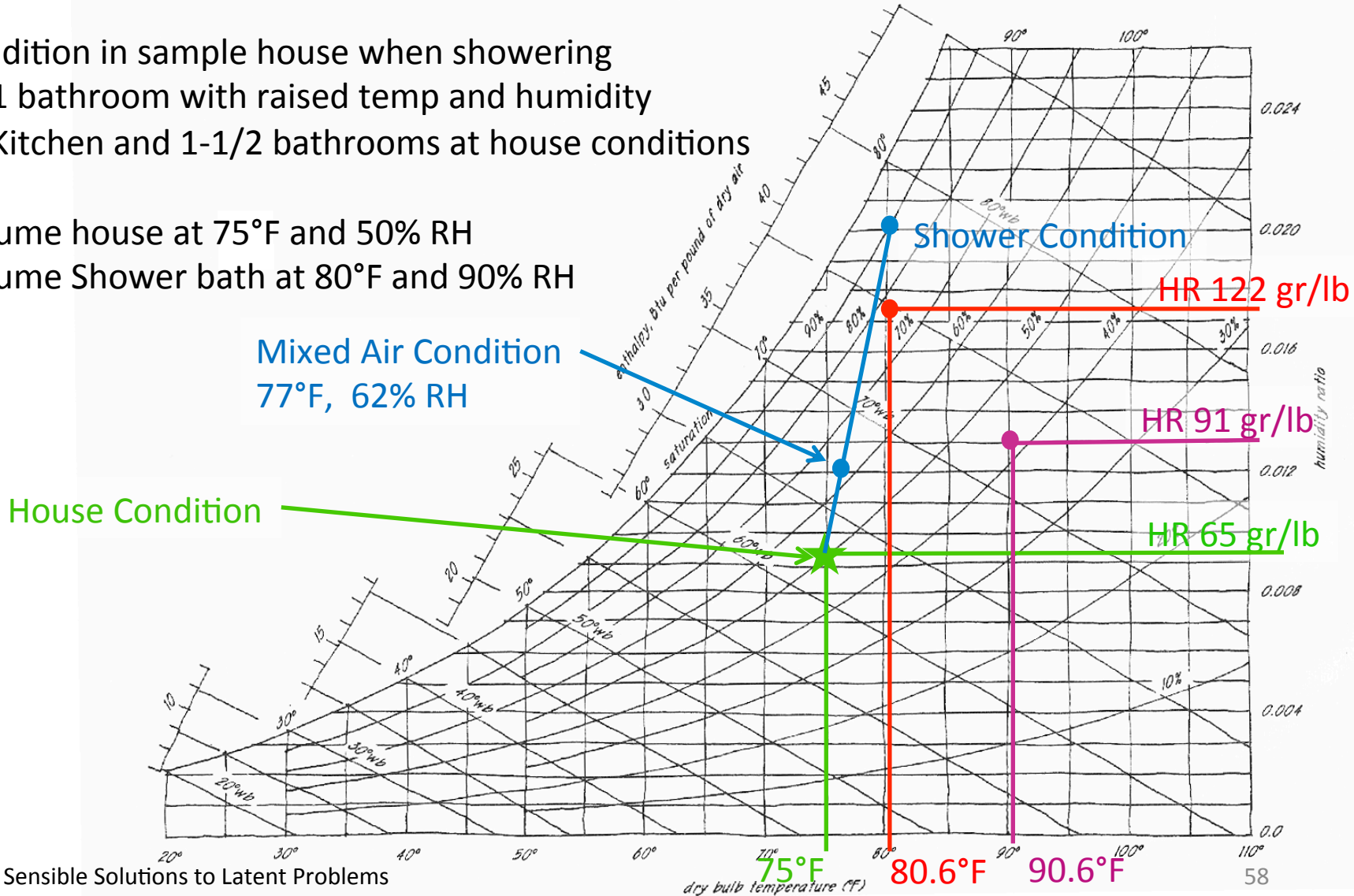
Should ERVs ventilate bathrooms?

Condition in sample house when showering

- 1 bathroom with raised temp and humidity
- Kitchen and 1-1/2 bathrooms at house conditions

Assume house at 75°F and 50% RH

Assume Shower bath at 80°F and 90% RH



Mitigation Strategies: Heat Pumps

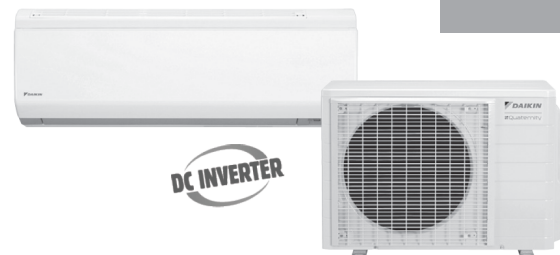
Popular in low load buildings

- Provide heating and cooling (& dehumidify)
- Energy efficient
- Relatively simple installation

Limitations

- Primarily designed for cooling
- Hard to estimate part-load moisture removal
- SHR is dependent upon conditions and air flow

“So the rated SHR of any unit is, in my view an entirely unsatisfactory and unproductively theoretical misimpression of actual DH performance.” - Lew Harriman



Heat Pumps with Dry Mode

Both Mitsubishi & Fujitsu (likely others) have “Dry Mode” operation

- Reduces airflow over the evaporator (cooling) coil
- Maintains coil temp at slightly below dew point
- Attempts to dehumidify with the minimal amount of cooling

For 3/4 ton to 1-1/4 ton heat pumps:

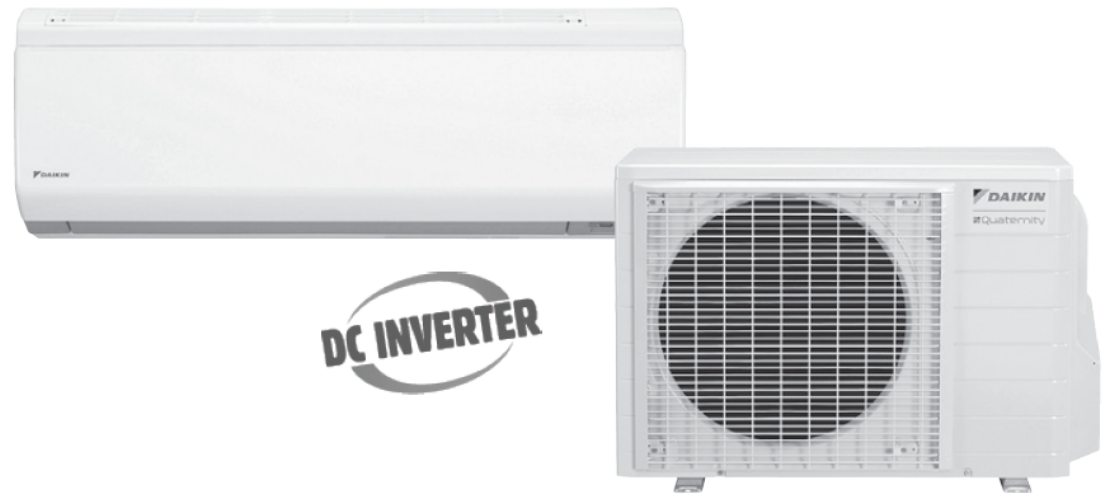
- Mitsubishi SHR range from 0.92 – 0.7
- Fujitsu 2.6 – 4.0 pint/hour
 - Approx. SHR range 0.71 – 0.78



Heat Pump Acting Like a Dehumidifier

Daikin has **Quaternary** model with dehumidification mode

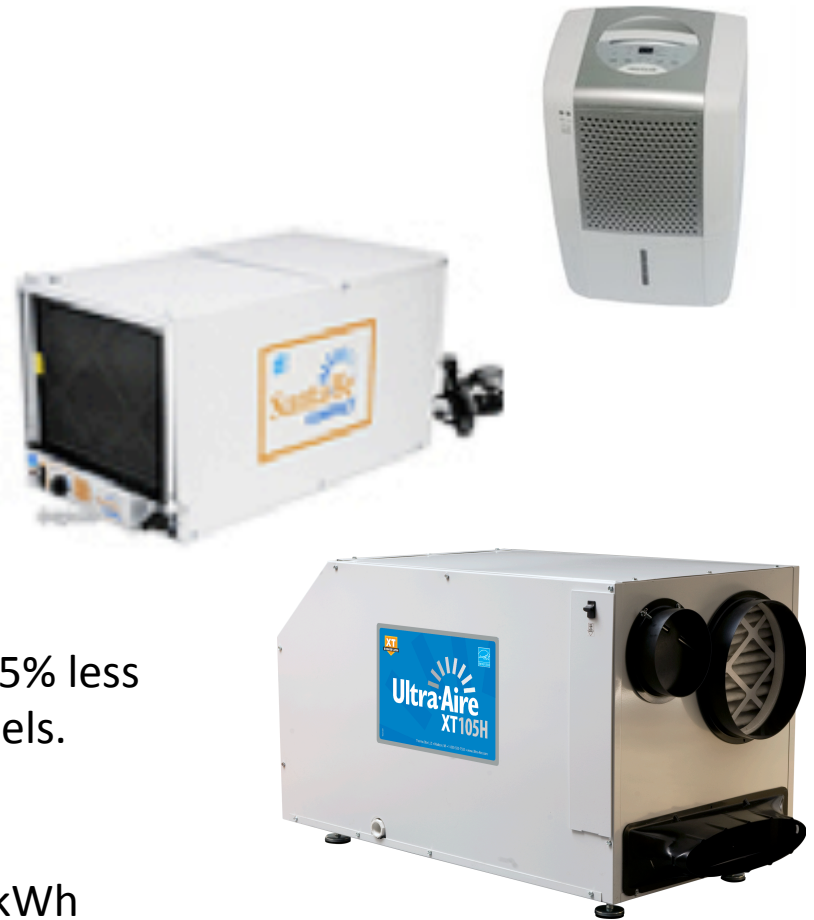
- Can set and monitor relative humidity levels
- Has a reheat coil to prevent overcooling
- Lists dehumidification capacity of 3.3 – 4.8 pints/hour



Mitigation Strategy: Dehumidifiers

Use the same basic technology as AC Units with 2 main differences:

- Designed for dehumidification
 - Relative humidity set point
 - Deeper coil
 - Lower air flow
- Condenser coil (heat rejection) inside
 - Heaters!



For EnergyStar rating must use 15% less energy than “conventional” models.

Large variability:
range from 1.85 L/kWh to 4.2 L/kWh

Stand-alone Dehumidifiers

Good solution for damp basements and finished basements

- Large thermal mass mitigates heat rejection
- Warmer and drier can be a benefit to these spaces even in summer months



Can also work in remainder of the house
If located properly

- Locate near ducted heating/cooling system return and run air handler fan for distributing dry air
- Can mitigate the heat rejection by dispersing it.



Whole House Dehumidifiers

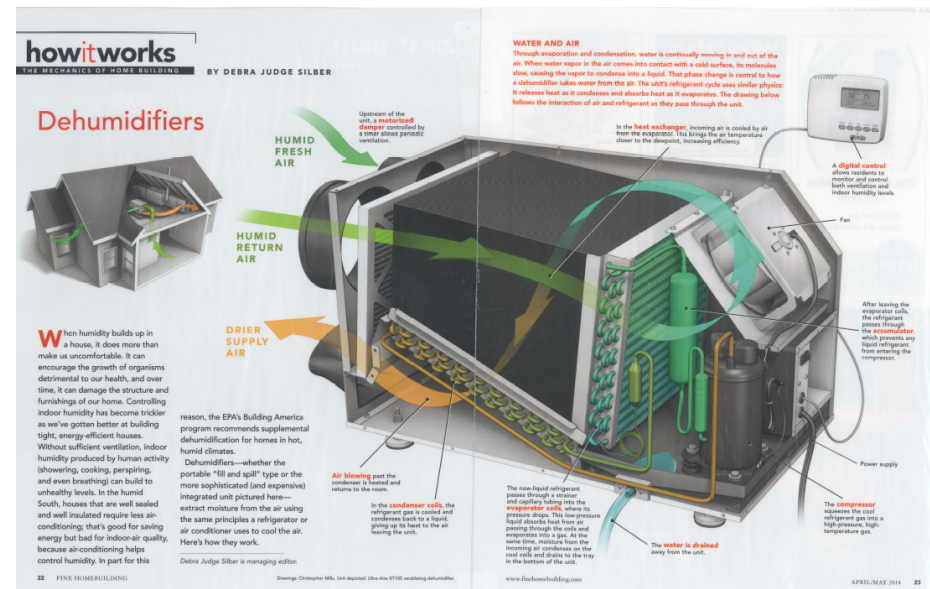
Ducted solution for whole house dehumidification

- Distributing to whole house can help mitigate the heat rejection
- Will increase the sensible load when running.
- Has ventilation intake port so can *possibly* be coupled with ERV supply air distribution with careful planning.



Ultra-Aire has highest efficiency models

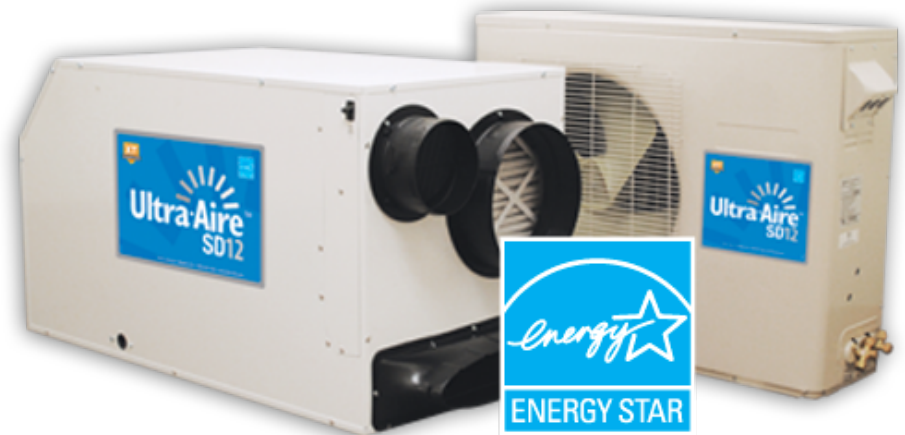
- Utilizes and air to air heat exchanger to pre-cool air and reduce compressor power consumption.



Whole House Split-Dehumidifiers

Ducted split-system solution for whole house dehumidification

- Heat rejection to the outside so also provides some sensible cooling
- Rated at 4,300 BTUH sensible and 7.7 pints/hr latent SRE ~ 0.34
- Has ventilation intake port so can *possibly* be coupled with ERV supply air distribution with careful planning.
- For low-load house may be an excellent cooling/dehumidification solution but does not provide heating.



One Last Option...

